

Practical realization of chiral nonlinearity for strong topological protection

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Abstract

Nonlinear topology has been much less inquired compared to its linear counterpart. Existing advances have focused on nonlinearities of limited magnitudes and fairly homogeneous types. As such, the realizations have rarely been concerned with the requirements for nonlinearity. Here we explore nonlinear topological protection by determining nonlinear rules and demonstrate their relevance in real-world experiments. We take advantage of chiral symmetry and identify the condition for its continuation in general nonlinear environments. Applying it to one-dimensional topological lattices, we can obtain definite evolution paths of zero-energy edge states that preserve topologically nontrivial phases regardless of the specifics of the chiral nonlinearities. Based on an acoustic prototype design, we theoretically, numerically, and experimentally showcase the nonlinear topological edge states that persist in all nonlinear degrees and directions without any frequency shift. Our findings unveil a broad family of nonlinearities compatible with topological non-triviality, establishing a solid ground for future drilling in the emergent field of nonlinear topology.

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23 1 Introduction

24 Topological protection has received a surge of interest owing to its strong immunity to para-
 25 metric perturbations and geometrical defects. It has been investigated on versatile platforms,
 26 from quantum mechanics [1] to multifarious classical realms such as electronics [2–5], pho-
 27 tonics [6–10] and phononics [11–20]. In contrast to the tremendous attention paid to linear
 28 physics and band theory, topological research has less accented on the intersections with non-
 29 linear dynamics [10, 21, 22], despite the ubiquity of nonlinearity in nature. The nonlinear
 30 sources exploited for topological purposes include varactor diodes inserted in electrical cir-
 31 cuits [4, 5, 23–25], optical materials with intensity-dependent refractive index [10, 26–28],
 32 geometry [29, 30] or nonlinear stiffness [31–33] of mechanical structures, and active means
 33 that create nonlinearity together with non-Hermiticity [34]. However, the types of nonlinear-
 34 ities are rather homogeneous in previous surveys, with a strong dominance of Kerr-like onsite
 35 nonlinearities [5, 6, 10, 23, 26, 27, 31, 33, 35–42], due to their ease in passive realizations and
 36 the link to bosonic quantum systems through the well-known Gross-Pitaevskii equation [43].
 37 Exceptions arise mainly from the use of specific lasers [28, 34] or electrical elements [4, 25],
 38 whose self-focusing or defocusing behaviors are described by saturable nonlinear gains.

39 The nonlinear effects, once triggered, have resulted in topologically nontrivial phases that
 40 were mostly trivial in the linear regime [10, 22], allowing for many fascinating phenom-
 41 ena such as first- or second-order topological insulators [5, 26, 32, 39], soliton propagation
 42 [27–29, 31, 37, 44, 45], and higher harmonic generations [24, 46–48]. Nevertheless, studies
 43 reported to date possess their own specific effective range of nonlinearities. Some of them have
 44 been restricted to weak nonlinear magnitudes to approach theoretical models and/or to en-
 45 able theoretical analyses (viable linearization and perturbation methods) [4, 5, 31, 35, 40, 46].
 46 Others, on the other hand, have required nonlinearity strong enough to activate nonlinear
 47 states (e.g., solitons) or to localize them clearly (e.g. corner topological states). A few have
 48 explored large intervals of nonlinear levels from low to high (before chaos), but with the
 49 edge modes/states shifted in frequency [23, 33, 36, 38, 49], ultimately destroying topological
 50 phases due to nonlinearity-induced symmetry breaking. Nonlinear topology, discovered within
 51 limited contents and extents of nonlinearity, has hardly been discussed from a fundamental
 52 nonlinear perspective thus far. That is, taking the stand on topological demands, what non-
 53 linearities are actually needed? Is it feasible in practice to keep topological attributes intact

54 across all nonlinear magnitudes?

55 To tackle the question, here we unlock limitations to the manipulation of nonlinear topo-
 56 logical systems in theory and practice, by satisfying a symmetry that maintains topological
 57 non-triviality permanently. Different types of symmetries can enable topological phases of
 58 matter [6, 12, 50], including time-reversal symmetry [50], reflection symmetry [51], Parity-
 59 Time symmetry [34], chiral symmetry [52, 53] or derived sub-symmetries [54]. Our study
 60 utilizes chiral symmetry that is closely related to the emergence of zero-energy topological
 61 edge states [55]. We first identify the nonlinear condition for symmetry preservation in gen-
 62 eral periodic systems. We then introduce eligible nonlinearities in one-dimensional (1D) lat-
 63 tices to alter the linearly produced stationary topological edge states. Their variations are
 64 qualitatively predictable assuming chiral nonlinearities with general monotonic dependence
 65 on amplitudes. A concrete nonlinear case is finally examined in a theoretical lumped element
 66 circuit and in the equivalent real active nonlinear acoustic system. We confirm theoretically,
 67 numerically, and experimentally that under chiral symmetry, nonlinear edge states can sustain
 68 their topologically nontrivial phases while never shifting in frequency.

69 2 Chiral symmetry for general nonlinear periodic systems

70 In terms of the Hamiltonian \mathbf{H} of the system, and in the presence of arbitrary nonlinearities and
 71 non-localities depending on the different degrees of freedom (a_i, b_j, c_k, \dots) contained in the
 72 system, chiral symmetry implies that $\Gamma \mathbf{H}(a_i, b_j, c_k, \dots) \Gamma^\dagger = -\mathbf{H}(a_i, b_j, c_k, \dots)$, with Γ the chiral
 73 operator and \dagger the conjugate transpose [53]. In the chiral base of the degrees of freedom,
 74 where $\Gamma = \begin{bmatrix} 1_a & 0 \\ 0 & -1_b \end{bmatrix}$ with 1_a and 1_b the identity matrices of random sizes, this definition is
 75 equivalent to say that $\mathbf{H}(a_i, b_j, c_k, \dots)$ is block off-diagonal, namely

$$\mathbf{H}(a_i, b_j, c_k, \dots) = \begin{bmatrix} 0 & h(a_i, b_j, c_k, \dots) \\ h^\dagger(a_i, b_j, c_k, \dots) & 0 \end{bmatrix}. \quad (1)$$

76 Notably, there are no specific restrictions on the nonlinearities in $h(a_i, b_j, c_k, \dots)$ in Eq. (1).
 77 They can, in principle, take any form, and rely randomly on the system elements, even in a
 78 non-local way. The only requirement is that the sites of the same chirality must be uncoupled
 79 from each other. Conversely, any nonlinearity that creates couplings among them will in-
 80 evitably cause symmetry breaking, as is the case with the extensively inquired Kerr-like onsite
 81 nonlinearity [5, 6, 10, 23, 26, 27, 33, 35–42].

82 3 Generalized nonlinear topological protection with chiral sym- 83 metry

84 The satisfaction of Eq. (1) allows for chiral symmetry in Hamiltonians of any dimension. For
 85 a direct application, we focus on the zero-energy edge states in 1D dimerized lattices, where
 86 Eq. (1) is already met by the 2x2 Hamiltonian in the natural base. We start with the linear
 87 chiral case, for which, the recurrent relations read: $\eta_L a_n + a_{n+1} = 0$ and $\eta_L b_n + b_{n-1} = 0$,
 88 where a_n and b_n are the amplitudes of the two sites of the n-th unit cell, and the N sites a_n
 89 (b_n) constitute the entire sublattice A (B) of the system. A topologically nontrivial phase is
 90 obtained if the hopping ratio η_L (ratio between the hopping terms) is smaller than one. The
 91 resulting linear topological edge state is displayed in Fig. 1, where the sites a_n carry a decrease
 92 in amplitudes along A, with the descent rate fixed by η_L . The presence of chiral symmetry
 93 makes the sites b_n stay stationary, independent of a_n .

94 When nonlinearities get involved in a way that respects Eq. (1), the system energy relations
 95 read:

$$0 = a_{n+1} + [\eta_L + \eta_{\text{NL}a}(a_{n+i}, b_{n+j})] a_n, \quad 0 = b_{n-1} + [\eta_L + \eta_{\text{NL}b}(a_{n+k}, b_{n+l})] b_n, \quad (2)$$

96 This suggests that, under chiral symmetry, the participation of nonlinearity results only in
 97 modifications in the hopping ratios. They are transformed from the linear invariant η_L to the
 98 amplitude-dependent nonlinear variables $\eta_L + \eta_{\text{NL}a}(a_{n+i}, b_{n+j})$ applied to a_n and $\eta_L + \eta_{\text{NL}b}(a_{n+k}, b_{n+l})$
 99 applied to b_n . a_{n+i} and b_{n+j} (a_{n+k} and b_{n+l}) refer to each site that the nonlinearity in $\eta_{\text{NL}a}$
 100 ($\eta_{\text{NL}b}$) depends on. They can be arbitrary in the system, i.e., the integer i or j or k or l can be
 101 zero if the dependency occurs within the n -th unit cell, or nonzero if the dependency is on the
 102 other interacting unit cells.

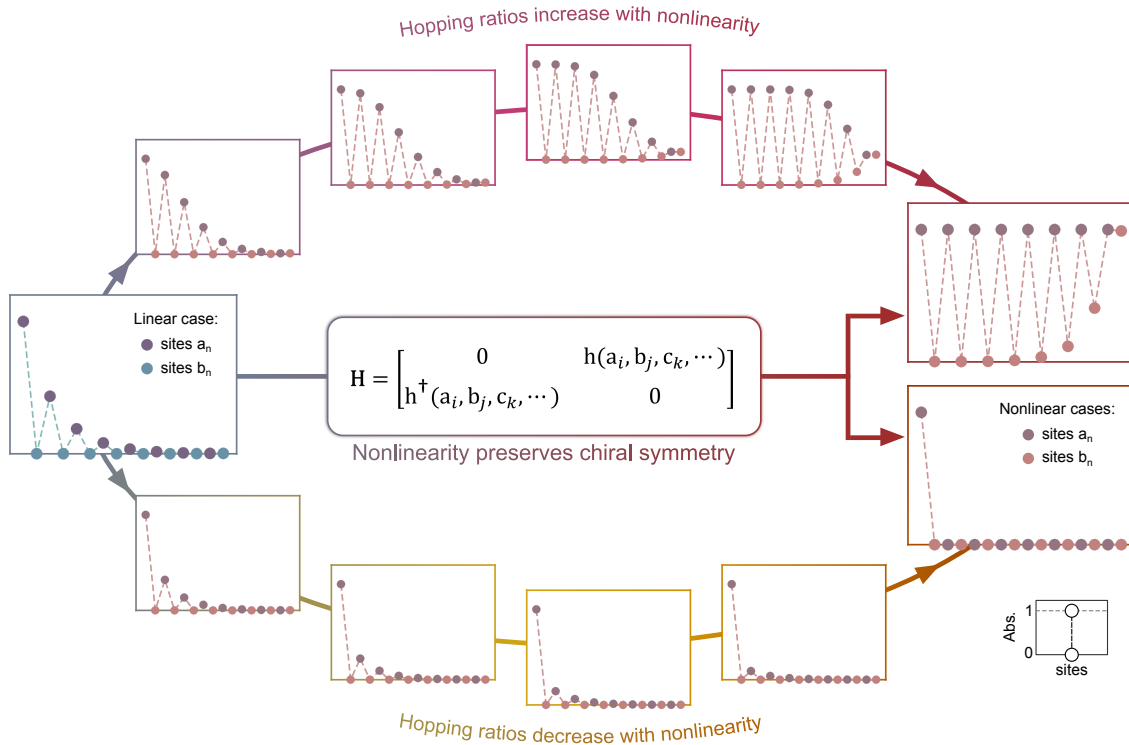


Figure 1: **Qualitative estimations of the evolution laws for zero-energy edge states in 1D dimerized systems with symmetry-preserving nonlinearities.** Profiles of the zero-energy edge state that is initially (linearly) topological and then varied as chiral nonlinearities increase and decrease the hopping ratios on sublattice A, respectively. In each profile, the amplitude of the first site a_1 is fixed at 1. The requirement on the Hamiltonian H is explained in Eq. (1). The variation trends apply to the entire class of nonlinearities that lead to monotonic changes in the hopping ratios as the site amplitudes increase.

103 Unlike a previous theoretical study discussing one particular form of nonlinearity [53],
 104 here we predict edge state variations under generalized chiral nonlinearities and validate them
 105 experimentally. We consider the most common relationship between site amplitude and non-
 106 linear effects, namely nonlinearities cause monotonic changes in the hopping ratios with in-
 107 creasing site amplitudes. A broad range of classical nonlinearities satisfy this condition, from
 108 polynomial laws (quadratic or cubic, etc.) to saturable effects. In addition, non-linear laws
 109 are not restricted to local effects. We first deal with nonlinearities that are positively cor-
 110 related with amplitudes. Based on $a_n > a_{n+1}$ of the linear state, these nonlinearities lead
 111 to $|\eta_{\text{NL}a}(a_{n+i}, b_{n+j})| > |\eta_{\text{NL}a}(a_{n+1+i}, b_{n+1+j})|$ in the early nonlinear stage (negligible effects
 112 of sites in B, since they carry zero amplitude initially), where the sign of $\eta_{\text{NL}a}$ determines
 113 whether nonlinearity increases or decreases the hopping ratios on A. If $\eta_{\text{NL}a} < 0$, we have
 114 $\eta_L + \eta_{\text{NL}a}(a_{n+i}, b_{n+j}) < \eta_L + \eta_{\text{NL}a}(a_{n+1+i}, b_{n+1+j}) < \eta_L < 1$, i.e., the hopping ratios are di-
 115 minished by nonlinearity, with the decrement less and less along A. As nonlinearity is further
 116 strengthened, its positive dependence on amplitudes perpetuates the above law. The first hop-
 117 ping ratio remains thus the smallest, always yielding the largest reduction of amplitude from
 118 a_1 to a_2 . Following this trend, we reach a limit situation where solely the first site a_1 has a
 119 nonzero amplitude. The sites b_n in B remain at zero amplitude, owing to chiral symmetry
 120 and the fast decay of the nonlinear mode that prevents it from reaching the other end of the
 121 system. The total expected edge state variations for nonlinearity decreasing the hopping ratios
 122 on A ($\eta_{\text{NL}a} < 0$) are depicted graphically in the lower branch in Fig. 1.

123 The reasoning applies likewise to the opposite scenario of $\eta_{\text{NL}a} > 0$, where $|\eta_{\text{NL}a}(a_{n+i}, b_{n+j})|$
 124 $> |\eta_{\text{NL}a}(a_{n+1+i}, b_{n+1+j})|$ results in $\eta_L + \eta_{\text{NL}a}(a_{n+i}, b_{n+j}) > \eta_L + \eta_{\text{NL}a}(a_{n+1+i}, b_{n+1+j}) > \eta_L$.
 125 Namely the hopping ratios are increased by nonlinearity, with the increment smaller and
 126 smaller along A. Remarkably, the first ratio is the largest here, contrary to the previous case of
 127 $\eta_{\text{NL}a} < 0$. The enhancement of nonlinearity impels it to first attain 1, at which moment the site
 128 a_2 acquires the same amplitude as a_1 . After that, if nonlinearity still can increase the hopping
 129 ratio, a_2 exceeds a_1 in amplitude. The continuation along this direction makes the ascent of
 130 a_2 incessant and towards an infinite level, inevitably ending with the system instability. For
 131 this reason, to allow stable states at all nonlinear magnitudes, the nonlinearity should always
 132 keep the first hopping ratio at 1 once $a_2 = a_1$ is reached. The other hopping ratios follow the
 133 same result due to the periodicity of the system. That is, for $\eta_L + \eta_{\text{NL}a}(a_{n+i}, b_{n+j})$ applied to
 134 a_n , we have $\eta_L + \eta_{\text{NL}a}(a_{n+i}, b_{n+j}) = 1$ once $a_{n+1} = a_n$. Such a relationship easily holds if the
 135 nonlinear hopping terms for a_n and a_{n+1} are dominated by their site amplitudes, respectively,
 136 as exemplified by the explicit case in Fig. 2a (see Eqs. (A.5) and (A.6)). It shows that, as the
 137 nonlinearity strengthens, the sites a_n ($n \geq 2$) successively arrive at the amplitude of a_1 and
 138 then sustain there. Ultimately, they will exhibit the same amplitude, forming a 'plateau' in A.

139 For actual systems with finite dimensions, the zero-energy mode reaches the other edge
 140 of the system when all sites in A are nonlinearly endowed with nonzero amplitudes. In this
 141 case, the excited opposite zero mode causes the amplitude of the sites in B to begin to rise,
 142 with a lowering from b_n to b_{n-1} , i.e., a heightening along the structure. No conclusion can be
 143 drawn about the direction of changes in the hopping ratios on B. Their increase or decrease
 144 are separate from those on A, as Eq. (1) states. Despite this, it is certain that from an initial
 145 value of less than 1, the nonlinearity should drive the hopping ratios up to 1 at most, as
 146 we discovered earlier through the sublattice A. The extreme nonlinear result can hereby be
 147 extrapolated: sites b_n conduct an increase in amplitude along B, with merely the first b_1 at
 148 rest. Our overall estimates for the case of nonlinearity increasing the hopping ratios on A
 149 ($\eta_{\text{NL}a} > 0$) are delineated schematically in the upper branch in Fig. 1, where the pattern in B
 150 results from the explicit nonlinearity considered later in Fig. 2a.

151 Performing the same analysis as above for nonlinearities that are negatively correlated
 152 with site amplitudes, one will obtain the same evolution limits as in Fig. 1. Collectively, ac-

153 counting for a monotonic amplitude dependence of the chiral nonlinearity, the hopping ratios
 154 can always stay smaller than or at most equal to 1 for both sublattices A and B. Therefore,
 155 the derived variation tendencies lead to the nonlinear edge states that remain topologically
 156 nontrivial, whatever the nonlinear contents. A result similar to part of Fig. 1 was previously ob-
 157 served in a numerical attempt [31], but with a particular nonlinear management and without
 158 discussing the underlying symmetry cause. Distinctively, here our starting point is to interro-
 159 gate chiral symmetry, thus unveiling the entire class of nonlinearities that ensures topological
 160 non-triviality.

161 4 Example of nonlinear topological protection with chiral symme- 162 try

163 To confirm our anticipations in Fig. 1, we take the example of a concrete finite system repre-
 164 sented by the lumped element circuit in Fig. 2a. It consists of 8 unit cells, each with linear
 165 and nonlinear resonators. The linear resonators LF_{2k-1} and LF_{2k} are identical and exhibit a
 166 resonance at a lower frequency f_{LF} . The nonlinear resonators HF_{2k-1} and HF_{2k} resonate at the
 167 same frequency f_{HF} , higher than f_{LF} , while a larger (linear) resonance bandwidth is assigned
 168 to HF_{2k-1} compared to HF_{2k} . The generators $V_{2k-1}^{(NL)}$ ($V_{2k}^{(NL)}$) introduce nonlinearity into HF_{2k-1}
 169 (HF_{2k}), with the explicit nonlinear laws given also in Fig. 2a. The overall system allows sta-
 170 tionary topological edge states at two different frequencies (Appendix A.1, Fig. 4), dominated
 171 by the resonance of LF_n and HF_n ($n = 2k - 1$ and $2k$), respectively. The voltages carried by
 172 LF_{2k-1} (LF_{2k}) correspond to the amplitudes of sites a_n (b_n). In the linear regime, the hopping
 173 terms for a_n (b_n) and a_{n+1} (b_{n+1}) are directly mapped to the capacitances $C_{2k-1}^{(HF)}$ in HF_{2k-1} and
 174 $C_{2k}^{(HF)}$ in HF_{2k} . In the nonlinear regime, instead, they are dictated by the nonlinearity engaged.
 175 Their amplitude dependence is complex: it is not only on the sites a_n and b_n inside the asso-
 176 ciated n -th unit cell, but also on the sites b_{n-1} and a_{n+1} in the adjacent ones (Eqs. (A.5) and
 177 (A.6)). Despite this complexity, the chosen nonlinearities are rigorously chiral.

178 Our attention is devoted to the topological edge state where the resonance of HF_n prevails.
 179 Its nonlinear evolution is revealed in Fig. 2b. In the initial linear scenario, the hopping ratio
 180 is defined at around 0.41 (equal to $C_{2k}^{(HF)}/C_{2k-1}^{(HF)}$). The edge state frequency f_H is recognized
 181 from the site spectra in Fig. 2b, at the zero amplitudes of all sites b_n . Nonlinearity is then
 182 triggered and prescribed using the constant parameter G_{NL} in the nonlinear law. When G_{NL}
 183 is decreased along negative values, the hopping ratios on sublattice A are gradually enlarged.
 184 The first ratio keeps receiving the greatest increment. It takes the lead to reach 1, followed by
 185 the others in succession. At the very end, the plateau on A is infinitely approached, with solely
 186 the last hopping ratio still small. Conversely, in the direction $G_{NL} > 0$, nonlinearity incessantly
 187 reduces the hopping ratios on A. The relative descent (with respect to the former site) of a_2
 188 remains the largest compared to the other sites. The extreme case of only a_1 surviving is also
 189 attained. As for the sites b_n in B, their amplitudes rise exclusively after the activation of the
 190 opposite zero mode (along $G_{NL} < 0$), presenting the expected increasing order from b_1 to b_8 .

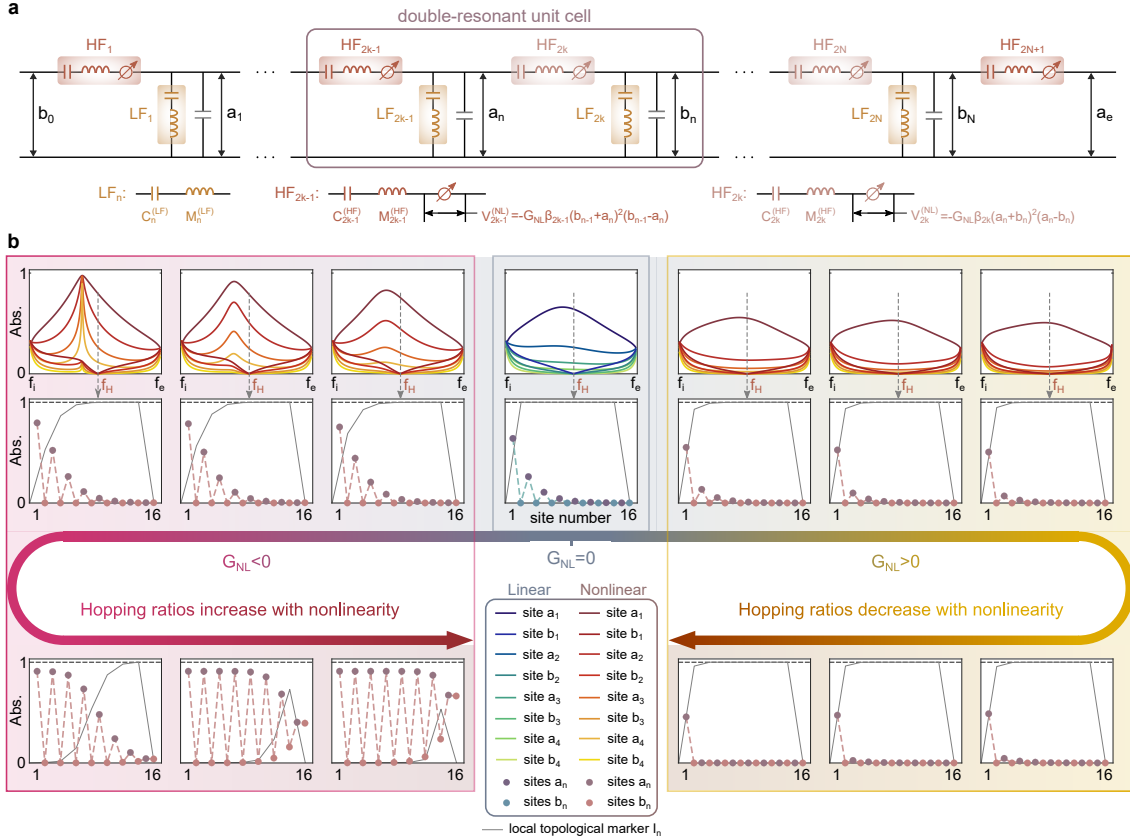


Figure 2: Evolution of the chiral symmetry protected nonlinear topological edge states: theoretical demonstration in a lumped element circuit with coupled resonators. (a) The considered 1D nonlinear system. It is made of 8 unit cells, each composed of 2 linear resonators LF_n and 2 nonlinear resonators HF_n ($n = 2k - 1$ and $2k$) where nonlinearity is added through the generators $V_n^{(NL)}$. (b) Nonlinear variations of the linearly generated stationary topological edge state, under the intervention of the nonlinearity given in (a). The nonlinear levels and directions are tuned by the constant parameter G_{NL} in the nonlinear law. It increases (decreases) the hopping ratios on sublattice A with $G_{NL} < 0$ ($G_{NL} > 0$). The edge state frequency f_H is identified from the spectra of a_n and b_n ($n = 1, 2, 3, 4$) in the frequency range of $[f_i, f_e]$. All the edge state amplitudes in (b) are normalized to the same value. They are obtained with the Harmonic Balance Method (Appendix A.3), and the results for more cases are summarized in Fig. 6. A time domain analysis with the time-integration method is outlined in Appendix B.1 (Fig. 7). In addition to the edge states, the local topological marker [53] \mathcal{I}_n (of the n -th unit cell, drawn at the location of each b_n) is equally displayed for each case (gray lines), which takes values between 0 (not topological) and 1 (topological, indicated by dashed lines).

211 To reveal the topological aspect of the system, we plot for each unit cell n , the local topological marker \mathcal{I}_n (Fig. 2b) that generalises in real space and for finite size systems, the bulk winding number of 1D chiral symmetric insulators [53]. This marker applies to the linearisation of Eq. (2) around a given nonlinear mode and captures the topology of small perturbations around it. It is particularly suitable for systems with inhomogeneous hopping amplitudes, such as ours, where the lattice translation invariance breaks down and the usual bulk winding number, defined in the Brillouin zone, becomes inappropriate. At an interface between a topological region where $\mathcal{I}_n = 1$ and a topologically trivial region where $\mathcal{I}_n = 0$, the linearised system also develops a zero-energy mode. Due to chiral symmetry, smoothly increasing the amplitude of the nonlinear edge state amounts to adding this linearized zero-mode to the nonlinear background zero-mode without changing its frequency [53]. Therefore, high-amplitude nonlinear modes can be obtained by summing up linearized chiral-symmetry-protected topological zero modes captured by \mathcal{I}_n . When nonlinear magnitude is increased along $G_{\text{NL}} > 0$, the interface between the topological phase where $\mathcal{I}_n = 1$ and the edge where \mathcal{I}_n vanishes becomes sharper. The nonlinear edge mode is thus localized more and more on a single site at the edge. In contrast, when $G_{\text{NL}} < 0$, the high amplitude region is associated with a vanishing topological marker, indicating a trivial phase, while low amplitude regions are still topological. The interface zero mode is displaced toward the bulk with increasing nonlinear magnitude along $G_{\text{NL}} < 0$. Accordingly, the amplitude rise of the nonlinear mode also shifts toward the bulk, which further displaces the topological transition between $\mathcal{I}_n = 1$ and $\mathcal{I}_n = 0$ in a self-sustaining loop, leading to a plateau shape of the nonlinear edge state in the end.

212 We confirm with Fig. 2b that in our system, the chiral nonlinearities maintain the topological edge state at its linearly produced frequency f_{H} . Contrarily, if nonlinearity breaks the symmetry, the edge state loses its topological features: its amplitude rises on both sublattices A and B, and its frequency shifts away from f_{H} (see Figs. 8, 10 and 14 in Appendix B). The site spectra in Fig. 2b evidence in addition that the amplitude relation of $a_{n+1} < a_n$ is linearly valid over the entire frequency range of $[f_i, f_e]$ displayed therein. It can be nonlinearly transformed up to $a_{n+1} = a_n$ only, as the state at f_{H} shows. Not surprisingly, if nonlinearity is further enhanced from an already reached $a_{n+1} = a_n$, instability would occur at the related frequency. The leftmost spectra in Fig. 2b corresponds to the stability limit of this situation, where the site a_1 is caught up by a_2 at a frequency different from f_{H} . However, the nonlinear edge state at f_{H} is perpetually stable, since its variations always satisfy $a_{n+1} \leq a_n$. Collectively, the nonlinear results in Fig. 2b fully demonstrate our inferences for the general context of nonlinearity.

224 5 Experimental validations

225 After exploration of the theoretical lattice (Fig. 2), an equivalent active nonlinear acoustic system is adopted for experimental validation (Fig. 3a). A waveguide is used for connecting all the elements. Passive Helmholtz resonators are mounted on its (top) side to play the role of the linear LF_n , while electrodynamic loudspeakers are inserted inside and are actively controlled to act as the nonlinear HF_n . The control for each loudspeaker involves a feedback loop, where a nonlinear control law is appropriately defined based on the acoustic pressures measured on both faces of the loudspeaker membrane (Appendix A.6 and Fig. 11). The control output is returned to the loudspeaker terminals in real-time in the form of a drive current, achieving active resonators HF_n with fully adjustable and reconfigurable characteristics. A total of 8 unit cells are constructed in experiments, each composed of two equally spaced Helmholtz resonators and two equally spaced active loudspeakers. The sub-wavelength portions of tube V_a , enclosed by adjacent speakers, behave similarly to capacitors. Accordingly, the system in Fig. 3a realizes the theoretical lattice in Fig. 2a.

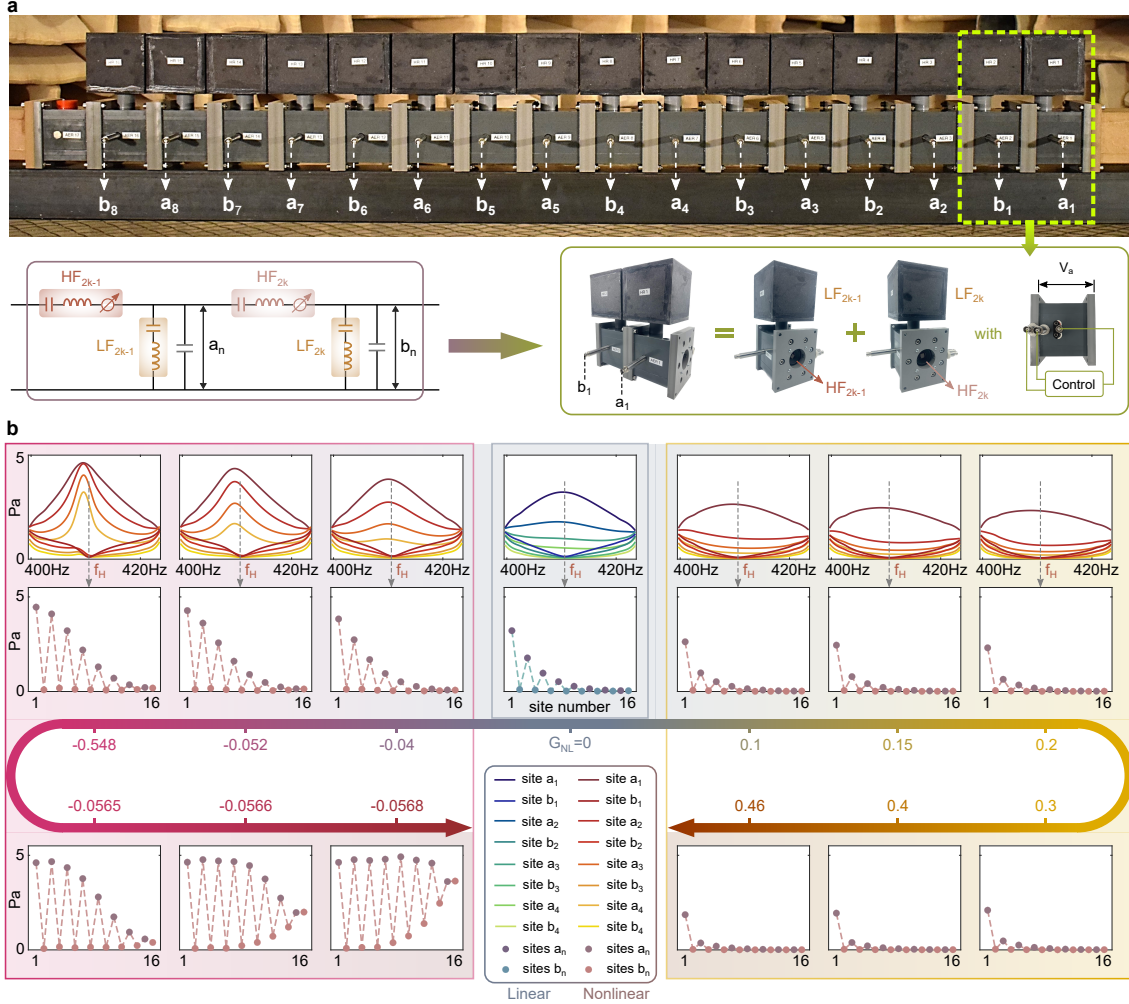


Figure 3: Evolution of the chiral symmetry protected nonlinear topological edge state: experimental validation in an active nonlinear acoustic system. (a) The actual system that realizes the theoretical lattice in Fig. 2a. The unit cell consists of two passive linear Helmholtz resonators (acting as LF_n) and two active nonlinear loudspeakers (acting as HF_n). The whole system starts and ends both with the controlled loudspeakers. The a_n and b_n correspond to the acoustic pressures applied to the Helmholtz resonators LF_{2k-1} and LF_{2k} , respectively. (b) Nonlinear topological edge states, measured as nonlinearity is progressively altered using the constant control parameter G_{NL} . The hopping ratios on sublattice A are increased (decreased) along $G_{NL} < 0$ ($G_{NL} > 0$). The edge state frequency f_H is identified from the spectra of a_i and b_i ($i = 1, 2, 3, 4$). Experimental results of more nonlinear cases are given in Fig. 13 in Appendix B.3.

238 The same investigations as in the theoretical studies are performed experimentally. First,
239 the topological edge state is successfully implemented in the linear case, as illustrated in Fig. 3b
240 (detailed linear results in Fig. 12 in Appendix B.3). A hopping ratio of around 0.54 is obtained,
241 not very far from the theoretical one of 0.41 (Fig. 2b). The discrepancy stems from the ap-
242 proximation of each space V_a as a lumped element (Appendix A.6). Based on the linear results,
243 nonlinearity is added to the system and tailored by the constant parameter G_{NL} , as theoret-
244 ically set in Fig. 2b. When nonlinear magnitude is reinforced along $G_{\text{NL}} < 0$, the hopping ratios
245 on A increase. The sites a_n sequentially attain the same level, enabling the theoretical plateau
246 limit at the greatest extent of nonlinearity. In the meantime of the ascent on sublattice A, the
247 sites in B first remain at rest and then rise in amplitude from the last one b_8 , which comply
248 also with the theoretical projections.

249 For nonlinearity decreasing the hopping ratios with $G_{\text{NL}} > 0$, the shape of the edge state
250 is centralized more and more on the structure (left) end, with all sites in B staying stationary.
251 The nonlinear variation along this direction proceeds until the first hopping ratio (the smallest
252 one) on A falls to about 0.2, with respect to the linear one of 0.54. The limit of only a_1 being
253 dynamic cannot be observed, as instability arises first, which is in accordance with time-domain
254 analysis (Appendix B.2, Fig. 9). Nevertheless, all expected laws of variations are exhaustively
255 justified by experiments. The realized nonlinear topological edge states are negligibly affected
256 by losses in the system. They preserve topologically nontrivial phases and with unchanged
257 frequency at f_{H} , since chiral symmetry is here rigorously obeyed by nonlinearity.

258 6 Conclusion

259 In this study, we explored the nonlinear possibilities for the persistence of topological non-
260 triviality. We targeted the symmetry-protected topological class and put the emphasis on chiral
261 symmetry. The condition to secure symmetry was first formulated for general nonlinear peri-
262 odic systems. It was then applied to one-dimensional lattices in which zero-energy topological
263 edge states were modified by arbitrary nonlinearities with chiral symmetry. The trajectories
264 of their nonlinear evolution were predicted based on a monotonic amplitude dependence of
265 the nonlinearities. The results show that chiral nonlinearities can consistently maintain the
266 edge states in a topologically nontrivial phase, regardless of the explicit nonlinear form and
267 magnitude. The derived nonlinear topological edge states were put into practice through the
268 consideration of a concrete finite system, with theoretical representation in a lumped element
269 circuit, and with numerical (Supplementary Materials, Section S2) and experimental imple-
270 mentations in an equivalent active nonlinear acoustic system. By virtue of chiral symmetry,
271 our investigations reveal a broad class of nonlinearities that keep the topological attributes in-
272 tact and the edge state frequency unshifted across all nonlinear magnitudes, opening up new
273 avenues of thought for the continued study of nonlinear topology.

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275 **Author contributions** R.F. and P.D. initiated and supervised the project. H.L. supervised
276 the experimental work. X.G. established the theoretical modeling, performed the numerical
277 simulations, designed the prototype, and carried out the measurements and data analysis. X.G.
278 and M.P. set up the experiment. L.J. and P.D. developed the theory. X.G. and H.L. raised part
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284 A Methods

285 A.1 Achievement of a topological system with chiral symmetry

286 The dynamics of the lumped-element circuit in Fig. 2a is described by

$$\begin{cases} \Delta_t^{(\text{HF})} q_{2k-1} = C_{2k-1}^{(\text{HF})} (b_{n-1} - a_n) + G_{\text{NL}} C^{(\text{HF})} (b_{n-1} + a_n)^2 (b_{n-1} - a_n), \\ \Delta_t^{(\text{HF})} q_{2k} = C_{2k}^{(\text{HF})} (a_n - b_n) - G_{\text{NL}} C^{(\text{HF})} (a_n + b_n)^2 (a_n - b_n), \\ \Delta_t^{(\text{LF})} (q_{2k-1} - q_{2k} - q_{2k-1}^{(a)}) = C_{2k-1}^{(\text{LF})} a_n, \\ \Delta_t^{(\text{LF})} (q_{2k} - q_{2k+1} - q_{2k}^{(a)}) = C_{2k}^{(\text{LF})} b_n, \end{cases} \quad (\text{A.1})$$

287 where $C^{(\text{HF})}$ is the average of the capacitors $C_{2k-1}^{(\text{HF})}$ and $C_{2k}^{(\text{HF})}$.

288 The time-domain variables in Eq. A.1 are:

289 (I) The q_{2k-1} , q_{2k} and $q_n^{(a)}$ ($n = 2k-1$ and $n = 2k$), which denote the charges of the resonators
 290 HF_{2k-1} , HF_{2k} and the capacitor C_a in parallel with LF_n , respectively.

291 (II) The voltages applied to LF_{2k-1} and LF_{2k} , which correspond to the time responses of a_n and
 292 b_n in the topological dimerized lattice. The site amplitudes of the edge states in Fig. 2b are
 293 extracted at the frequency of the fundamental component, while higher harmonic generations
 294 are negligible in our system (less than 1% in all cases).

295 (III) The generators $V_{2k-1}^{(\text{NL})}$ and $V_{2k}^{(\text{NL})}$, which deliver voltages that comply with the desired non-
 296 linearity given in Fig. 2a.

297 (IV), The time-domain differential operators $\Delta_t^{(\text{HF})}$ and $\Delta_t^{(\text{LF})}$, which read

$$\begin{cases} \Delta_t^{(\text{HF})} = \left[M_{2k-1}^{(\text{HF})} C_{2k-1}^{(\text{HF})} \frac{d^2}{dt^2} + 1 \right] = \left[M_{2k}^{(\text{HF})} C_{2k}^{(\text{HF})} \frac{d^2}{dt^2} + 1 \right], \\ \Delta_t^{(\text{LF})} = \left[M^{(\text{LF})} C^{(\text{LF})} \frac{d^2}{dt^2} + 1 \right]. \end{cases} \quad (\text{A.2})$$

298 Substituting Eq. (A.2) into Eq. (A.1) and eliminating all terms containing charges, the
 299 equations on voltages can be obtained as follows:

$$\begin{cases} \Delta_t a_n = \Delta_t^{(\text{LF})} \left[C_1^{(\text{HF})} b_{n-1} + C_2^{(\text{HF})} b_n - C_1^{(\text{HF})} V_{2k-1}^{(\text{NL})} + C_2^{(\text{HF})} V_{2k}^{(\text{NL})} \right], \\ \Delta_t b_n = \Delta_t^{(\text{LF})} \left[C_1^{(\text{HF})} a_{n+1} + C_2^{(\text{HF})} a_n + C_1^{(\text{HF})} V_{2k+1}^{(\text{NL})} - C_2^{(\text{HF})} V_{2k}^{(\text{NL})} \right], \end{cases} \quad (\text{A.3})$$

300 with $\Delta_t = \Delta_t^{(\text{HF})} \Delta_t^{(\text{LF})} C_a + \Delta_t^{(\text{HF})} C^{(\text{LF})} + 2C^{(\text{HF})} \Delta_t^{(\text{LF})}$, and with $C_1^{(\text{HF})} = C_{2k-1}^{(\text{HF})}$, $C_2^{(\text{HF})} = C_{2k}^{(\text{HF})}$,
 301 $C^{(\text{HF})} = (C_1^{(\text{HF})} + C_2^{(\text{HF})})/2$.

302 If $\Delta_t = 0$ is possible, then Eq. (A.3) leads to

$$\begin{cases} 0 = t_{1b}(b_{n-1}, a_n) b_{n-1} + t_{0b}(b_n, a_n) b_n, \\ 0 = t_{1a}(a_{n+1}, b_n) a_{n+1} + t_{0a}(a_n, b_n) a_n, \end{cases} \quad (\text{A.4})$$

303 The Eq. A.4 satisfies the general description of 1D chiral topological systems in Eq. 2, where

304 the hopping terms t_{1b} , t_{1b} , t_{1b} and t_{1b} are expressed explicitly as follows,

$$\begin{cases} t_{1a}(a_{n+1}, b_n) = C_1^{(\text{HF})} + G_{\text{NL}} C^{(\text{HF})} (a_{n+1}^2 + b_n a_{n+1} - b_n^2), \\ t_{0a}(a_n, b_n) = C_2^{(\text{HF})} - G_{\text{NL}} C^{(\text{HF})} (a_n^2 + b_n a_n - b_n^2), \\ t_{1b}(b_{n-1}, a_n) = C_1^{(\text{HF})} + G_{\text{NL}} C^{(\text{HF})} (b_{n-1}^2 + a_n b_{n-1} - a_n^2), \\ t_{0b}(b_n, a_n) = C_2^{(\text{HF})} - G_{\text{NL}} C^{(\text{HF})} (b_n^2 + a_n b_n - a_n^2), \end{cases} \quad (\text{A.5})$$

305 with $C_1^{(\text{HF})} = C_{2k-1}^{(\text{HF})}$ and $C_2^{(\text{HF})} = C_{2k}^{(\text{HF})}$. Accordingly, the hopping ratios $\eta_L + \eta_{\text{NL}a}$ and $\eta_L + \eta_{\text{NL}b}$
306 can be obtained from

$$\eta_L + \eta_{\text{NL}a} = \frac{t_{0a}(a_n, b_n)}{t_{1a}(a_{n+1}, b_n)}, \quad \eta_L + \eta_{\text{NL}b} = \frac{t_{0b}(b_n, a_n)}{t_{1b}(b_{n-1}, a_n)}. \quad (\text{A.6})$$

307 The derivation from Eq. (A.3) to (A.4) implies that, if the higher harmonic generations are
308 negligible in the system, topological edge states can be achieved at the fundamental frequen-
309 cies in the presence of a solution for $\Delta_t = 0$. This is exactly the case in our system, where
310 the higher harmonic generations are consistently lower than 1%. All the edge state profiles
311 shown in this study refer to the absolute amplitudes of the fundamental components of a_n and
312 b_n . Interestingly, two frequencies allow $\Delta_t = 0$, i.e., the topological edge states are attained at
313 two different frequencies in our system, see Fig. 4 in Appendix B.1 for physical explanations.

314 A.2 Boundary conditions

315 Theoretically, for the edge state generations, we require that the boundaries b_0 and a_e of the
316 lumped element circuit in Fig. 2a satisfy $b_0 = a_e = 0$. However, this is not directly achievable
317 in practice, especially for the acoustic system we chose for the experiments. In our search for
318 applicable boundary conditions, we eventually found that the typical Non-Reflecting Bound-
319 ary Conditions (NRBCs) in planar acoustic wave propagation can replace the ideal ones, as
320 proved in Fig. 5 in Appendix B.1. They are thus undertaken for all the studies of the concrete
321 theoretical model and the equivalent experimental system.

322 A.3 Methods for theoretical solvings

323 To solve the problem associated with the circuit in Fig. 2a, we consider the original dynamic
324 equations in Eq. A.1 where all the variables are time-dependent. Two standard methods are
325 exploited for solving these nonlinear differential equations, namely the harmonic balance
326 method [56–58] and the time-integration method [59]. They are capable of handling strong
327 levels of nonlinearities, in contrast to the perturbation method and the method of multiple
328 scales that are valid only at weak nonlinearities.

329 The Harmonic Balance Method (HBM) refers to a semi-analytical method [56–58] which
330 determines the steady-state solutions of the nonlinear problem. The first 27 harmonics of each
331 variable are taken into account when solving Eq. A.1. The outcomes show that the higher har-
332 monic generations are lower than 1% in our system. The a_n and b_n in Fig. 2b correspond to the
333 absolute amplitudes of their fundamental harmonic components (at the edge state frequency
334 f_H). The detailed results (more nonlinear cases than in Fig. 2b) are summarised in Fig. 6 in
335 Appendix B.1.

336 The time integration method, with the fourth-order Runge-Kutta (RK4), is utilized to solve
337 the problem directly in the time domain, which accounts for the transient responses. The
338 relevant results are given in Fig. 7 in Appendix B.1.

339 A.4 Time-domain simulation of the experiments.

340 To better guide and analyze the experiments, we performed time-domain simulations for the
 341 active nonlinear acoustic system built in practice (Fig. 3a). The approach involves a Finite Dif-
 342 ference Time Domain (FDTD) method by discretization of the 1D wave equations. Practical
 343 details are accounted for in the simulations, that is (i) we consider the wave propagation inside
 344 each space between two nearby loudspeakers (with FDTD), (ii) we add the losses in all reso-
 345 nant elements and transmission lines according to the experimentally estimated values, (iii)
 346 the actual active control on each loudspeaker, with the control principle and laws explained
 347 in the following section for experiments (Eqs. (A.7) and (A.8) with $i(t)$ changing to $i(t - \tau)$,
 348 and with $\tau = 100 \mu s$). Regarding the numerical settings, we randomly take the experimental
 349 values of one loudspeaker to define all the others. The simulation outcomes are summed up
 350 in Fig. 9 in Appendix B.2. They are essentially identical to the experimental ones.

351 A.5 Characterisations of the experimental setup

352 In the experimental setup (Fig. 3a), the non-reflecting boundary conditions are achieved with
 353 anechoic terminations at both ends of the system, which are qualified by absorption coeffi-
 354 cients higher than 0.998 from 140 Hz (less than 5% of reflection). The waveguide refers to
 355 a PVC duct with a cross-sectional area of $6 \text{ cm} \times 6 \text{ cm}$, which ensures planar wave propaga-
 356 tion until 2.86 kHz. The manufactured Helmholtz resonators (labeled with HR_n in Fig. 3a)
 357 reach a transmission coefficient of around 0.008 at their resonance frequencies in the range of
 358 $[110.5 \text{ Hz}, 111.5 \text{ Hz}]$, corresponding to an acoustic resistance of $0.005 Z_c$ with Z_c the specific
 359 acoustic impedance of the air. The electrodynamic loudspeakers are all the same commer-
 360 cially available Visaton FRWS 5 SC model, while they possess different resonance frequencies
 361 (within $[345 \text{ Hz}, 375 \text{ Hz}]$) and bandwidths, which we calibrated beforehand.

362 A.6 Active control on the electrodynamic loudspeakers.

363 The loudspeaker membrane behaves as a mass-spring-damper system in the linear regime
 364 (weak input levels). The motion equation for its displacement ξ read

$$M_{ms} \frac{\partial^2}{\partial t^2} \xi(t) + R_{ms} \frac{\partial}{\partial t} \xi(t) + \frac{1}{C_{ms}} \xi(t) = p_{tot}(t) S_d - Bl i(t), \quad (\text{A.7})$$

365 In the passive open-circuit case, the membrane is subject to the total acoustic pressure p_{tot}
 366 over its effective surface area S_d , and the mechanical forces which rely on the mechanical
 367 mass M_{ms} , resistance R_{ms} , and compliance C_{ms} . Its dynamics are characterized by a specific
 368 acoustic impedance Z_s (ratio between acoustic pressure and velocity) in the frequency domain,
 369 $Z_s(j\omega) = \frac{1}{S_d} \left(j\omega M_{ms} + R_{ms} + \frac{1}{j\omega C_{ms}} \right)$.

370 The active control on each loudspeaker is implemented by specifying the current $i(t)$, which
 371 creates an electromagnetic force through the moving coil with a force factor of Bl . The control
 372 approach is depicted in detail in Fig. 11, where the control law is digitally defined with a
 373 Speedgoat real-time target machine manipulated in the Simulink environment of MATLAB. It
 374 produces the current $i(t)$ in the form of,

$$i(t) = \mathcal{F}^{-1} (\Phi(j\omega) \cdot P_{tot}(j\omega)) + \mathcal{F}^{-1} \left(\frac{S_d}{Bl} - \Phi(j\omega) \right) * \left((-1)^n \frac{C^{(exp)}}{C_n^{(exp)}} G_{NL} P_{tot}(t) (p_f(t) + p_b(t))^2 \right), \quad (\text{A.8})$$

375 where p_f and p_b are the acoustic pressures measured at the front and rear faces of the loud-
 376 speaker membrane, which are the two inputs for the control. \mathcal{F}^{-1} and the symbol $*$ designate
 377 the inverse of the Fourier Transform and the time convolution, respectively. The total acoustic

378 pressure p_{tot} reads $p_{\text{tot}} = p_f(t) - p_b(t)$, with $P_{\text{tot}} = \mathcal{F}(p_{\text{tot}})$ its Fourier transform. $C_n^{(\text{exp})}$ refers to
 379 the acoustic compliance achieved for the n -th loudspeaker which differs between $n = 2k - 1$
 380 and $n = 2k$, and $C^{(\text{exp})}$ is the average of two successive ones, they are equivalent to the elec-
 381 trical capacitors $C_1^{(\text{HF})}$ for $n = 2k - 1$, $C_2^{(\text{HF})}$ $n = 2k$, and $C^{(\text{HF})}$ in Eq. (A.1).

382 In Eq. (A.8), the linear part of control is represented by a linear transfer function $\Phi(j\omega)$,
 383 whereas the nonlinear part is determined by the parameter G_{NL} . For the linear part, $\Phi(j\omega)$ is
 384 used to tailor the impedance properties of the loudspeaker,

$$\Phi = \frac{S_d}{\text{Bl}} \cdot \beta \frac{Z_{\text{st}}(j\omega) - Z_s(j\omega)}{Z_{\text{st}}(j\omega)}. \quad (\text{A.9})$$

385 It targets a specific acoustic impedance $Z_{\text{st}}^{(\text{F})}$ with two degrees of freedom,

$$Z_{\text{st}}^{(\text{F})} = \frac{Z_{\text{st}} Z_s}{(1 - \beta) Z_{\text{st}} + \beta Z_s} = \left[\frac{1 - \beta}{Z_{\text{st}}} + \frac{\beta}{Z_s} \right]^{-1}, \quad (\text{A.10})$$

386 in which the control-designed impedance Z_{st} corresponds to a one-degree-of-freedom res-
 387 onator. It is made in parallel with the passive one Z_s , while their weights are adjusted by
 388 the constant parameter β .

389 For the control execution, there exists a time delay τ from control inputs to outputs, which
 390 is unavoidable in reality. It is taken into account in simulating the practical case by trans-
 391 forming $i(t)$ into $i(t - \tau)$ for Eq. (A.7), and is experimentally determined at $100 \mu\text{s}$. Since the
 392 loudspeakers are naturally different, the control time delay affects them differently, yielding
 393 discrepancies in control results. Nevertheless, the addition of the parameter β in the linear
 394 control law allows such an issue to be compensated for in experiments, by balancing between
 395 Z_{st} and Z_s . Fig. 12 in Appendix B.1 shows the results for linearly generated topological edge
 396 state.

397 As for the nonlinear part of the control law in Eq. (A.8), when the sub-wavelength cavity V_a
 398 between adjacent loudspeakers exhibits predominantly capacitor characteristics (the assump-
 399 tion under consideration, see Fig. 3a), we have $p_f = b_{n-1}$ and $p_b = a_n$ for loudspeakers with
 400 even indexes, and $p_f = a_n$ and $p_b = b_n$ for those with odd indexes. In this case, the nonlin-
 401 ear laws perfectly achieve the generators V_{2k-1}^{NL} and V_{2k}^{NL} required in the theoretical lattice in
 402 Fig. 2a.

403 Performing the above hybrid (linear and nonlinear) control on each loudspeaker, they all be-
 404 come Active Electroacoustic Resonators [60–63] (labeled with AER_n in Fig. 3a), presenting
 405 the desired properties for realizing HF_n . A low level of less than 1 Pa is maintained for sys-
 406 tem excitation. It ensures the linear behaviors of the loudspeakers in the passive (control off)
 407 regime. Thus, nonlinearity is generated and tuned in an exact way, i.e., through the active
 408 control only (using the constant parameter G_{NL} in the control law). The time responses of a_n
 409 and b_n are measured by the microphones below Helmholtz resonators, as indicated in Fig. 3a.
 410 The edge states shown in Fig. 3b refer to their components at the fundamental frequency (edge
 411 state frequency f_H). We confirm with measurements that the higher harmonic generations are
 412 consistently less than 1% in our acoustic system, which is in line with the theoretical model.
 413 The detailed experimental results of nonlinear topological edge states are provided in Fig. 13
 414 in Appendix B.3. The cases where nonlinearities break chiral symmetry are investigated in Ap-
 415 pendix B. Figs. 8, 10 and 14 show the corresponding theoretical, numerical, and experimental
 416 results, respectively.

417 B Supplementary results

418 Here in the Appendix B.1, B.2 and B.3, we show supplementary results for the theoretical study
419 of the lumped-element model in section 4, the time-domain simulation of the actual acoustic
420 system, and the experimental realization in section 5, respectively.

421 B.1 Theoretical results

422 This section includes:

423 Fig. 4: Principle and physical explanations for the generation of dual-band topological edge
424 states in our lumped-element system.

425 Fig. 5: Proof of the equivalence between the theoretically ideal boundary conditions (Fig. 5b)
426 and the non-reflecting ones (Fig. 5c) that are more realizable for our acoustic experiments.

427 Fig. 6: Detailed theoretical results obtained by solving Eq. (A.1) with the Harmonic Balance
428 Method (HBM). More cases are shown compared to Fig. 2 in the main text.

429 Fig. 7: Theoretical results obtained by solving solving Eq. (A.1) with the time integration
430 method (fourth-order Runge-Kutta).

431 Figs. 8: Theoretical results for two cases where nonlinearities break chiral symmetry. They are
432 in comparison with the simulation outcomes in Fig. 10 and the experimental ones in Fig. 14,
433 where the same forms of nonlinearities are considered.

434 B.2 Simulation results

435 This section includes

436 Fig. 9: Detailed time-domain simulation results of the realized nonlinear topological edge
437 states. Notably, practical situations are accounted for in the simulation (Appendix A.4), where
438 the pressure is not precisely homogeneous in the cavity, and the control uses the pressures close
439 to each loudspeaker as inputs (Appendix A.6). By contrast, the theoretical study assumes that
440 the cavity between successive HF_n behaves as a capacitor, thus presenting the same pressure
441 over it. This eventually causes a difference in hopping ratios in the two studies. In theoretical
442 results, the hopping ratio of the linear edge state is around 0.41, corresponding to the compli-
443 ance ratio between $C_2^{(\text{HF})}$ and $C_1^{(\text{HF})}$. Whereas the linear hopping ratio obtained in simulations
444 is equal to 0.52 (0.54 in experiments), larger than the theoretical value.

445 Fig. 10: Simulation results for two cases where nonlinearities break chiral symmetry. They are
446 in comparison with the theoretical ones in Fig. 8 and the experimental ones in Fig. 14, where
447 the same forms of nonlinearities are considered.

448 B.3 Experimental results

449 This section includes

450 Fig. 11: Principle of the real-time feedback control applied to electrodynamic loudspeakers.

451 Fig. 12: Experimental results of the topological edge state at f_H in the linear regime.

452 Fig. 13: Detailed experimental results of the realized nonlinear topological edge states. More
453 nonlinear cases are shown compared to Fig. 3.

454 Fig. 14: Experimental results for cases where nonlinearities break chiral symmetry. They are
455 in comparison with the theoretical ones in Fig. 8 and the simulation ones in Fig. 10, where the
456 same forms of nonlinearities are considered.

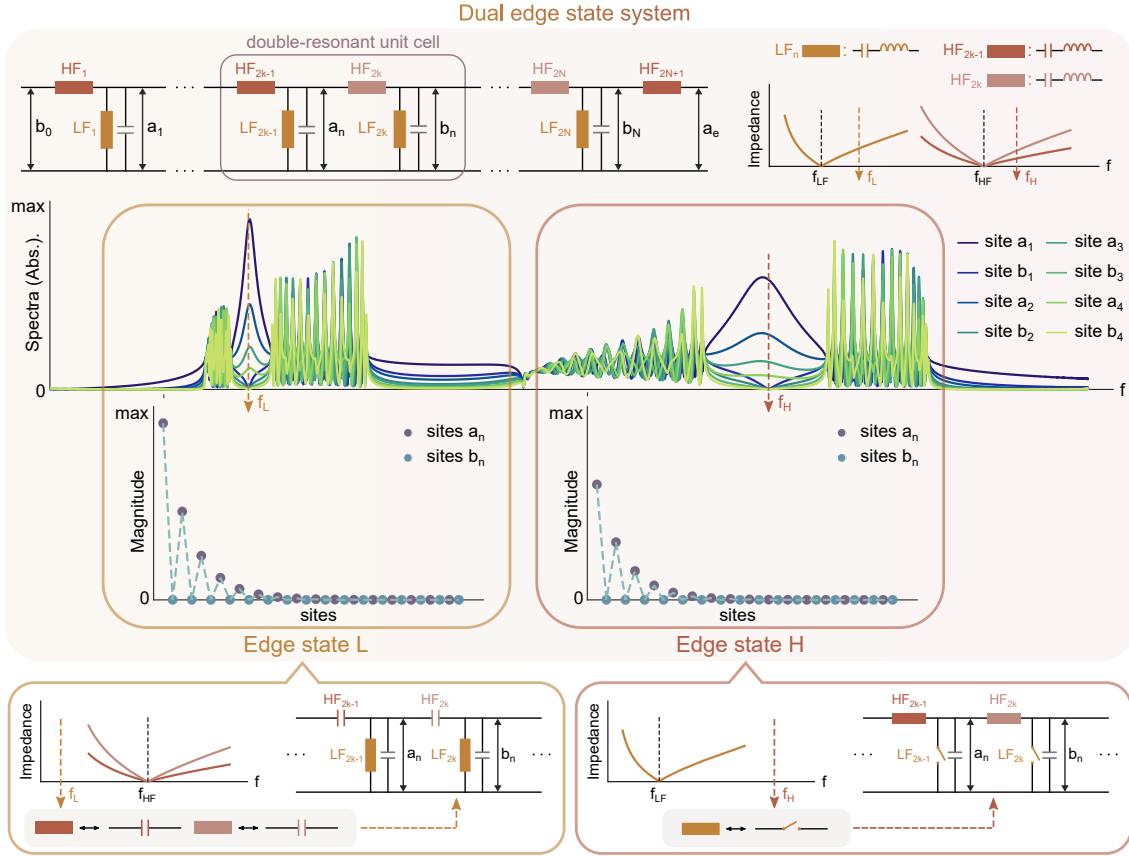


Figure 4: **Dual-band topological edge states in a single finite system.** Each unit cell (with index n) of the system includes 2 types of resonators, (i) identical resonators LF_n ($n = 2k-1$ and $2k$) resonating at a frequency f_{LF} , and (ii) resonators HF_n resonating at f_{HF} higher than f_{LF} , but with different resonance bandwidths between odd (HF_{2k-1}) and even (HF_{2k}) ones. In the linear regime where all HF_n possess no nonlinearities, with $f_{LF} < f_{HF}$, the resonators HF_n exhibit mainly capacitance characteristics in the vicinity of f_{LF} , leading to the manifestation of only the resonance of LF_n in the unit cell. Similarly, when close to the frequency f_{HF} which is far from f_{LF} , the resonators LF_n have barely any impact, only the resonance of HF_n can act. Therefore, our system is equivalent to a classic topological lattice made of single-resonant unit cells at two different frequencies, denoted as f_L and f_H , respectively, as delineated in this figure. Their mathematical derivations are provided in Appendix A.1. After introducing arbitrary nonlinearities, the linearly achieved topological edge states can persist and remain intact at these two frequencies, provided that the chiral symmetry is consistently satisfied, as we proved in the main text.

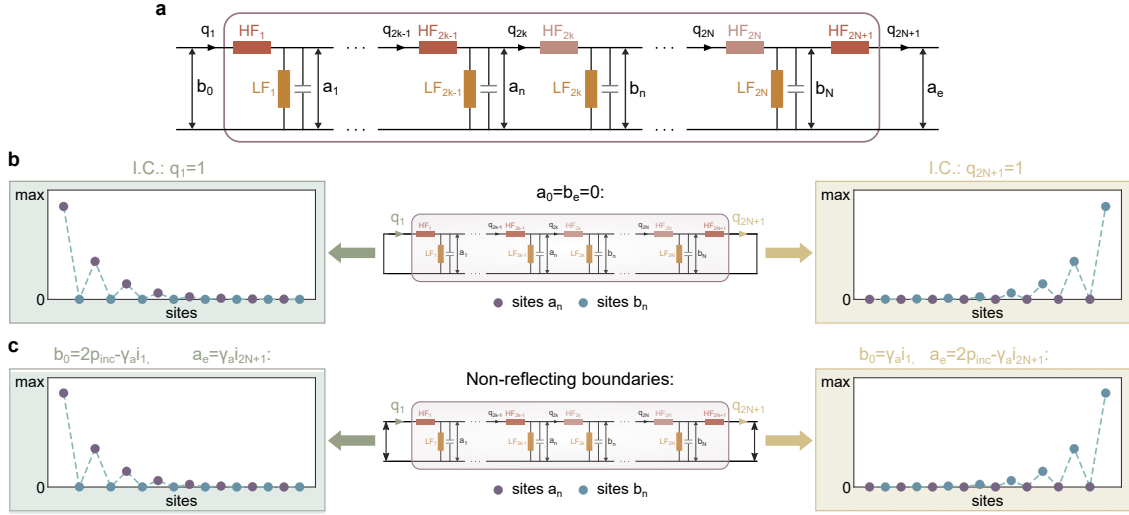


Figure 5: Identification of realizable boundary conditions. (a) The lumped element circuit considered, with b_0 and a_e the input and output boundaries, respectively. q_n designates the charge of the resonator HF_n . (b) Zero-energy topological edge state at f_H derived with the ideal closed-closed boundary conditions ($b_0 = a_e = 0$), and with a nonzero initial conditions of $q_1 \neq 0$ (left inset) or $q_{2N+1} \neq 0$ (right inset), respectively. (c) Zero-energy topological edge state at f_H derived with the Non-Reflecting Boundary Conditions (NRBCs) for both ends of the system, where excitation is defined at each end, respectively. Based on an electro-acoustic analog where electrical (voltage, current) is equivalent to acoustic (pressure, flow), NRBCs are translated into $a_e = \gamma_a i_{2N+1}$ ($b_0 = \gamma_a i_1$) for the right (left) end of the system, in which i_{2N+1} (i_1) represents the current circulating in HF_1 (HF_{2N+1}), and $\gamma_a = Z_c/S$ with Z_c the specific acoustic impedance of the air and S the surface area of the propagation medium. The planar wave excitation at the left (right) end of the system can be expressed by the total pressure in the form of $b_0 = 2p_{inc} - \gamma_a i_1$ ($a_e = 2p_{inc} - \gamma_a i_{2N+1}$), with p_{inc} the incoming source that comes from infinity (there is no reflection in the direction of incidence). All results are obtained with the 4-th order Runge-Kutta. They evidence the equivalence between the two types of boundary conditions. In this study, we opt for the NRBCs in (c) which is more realizable in our acoustic experiments.

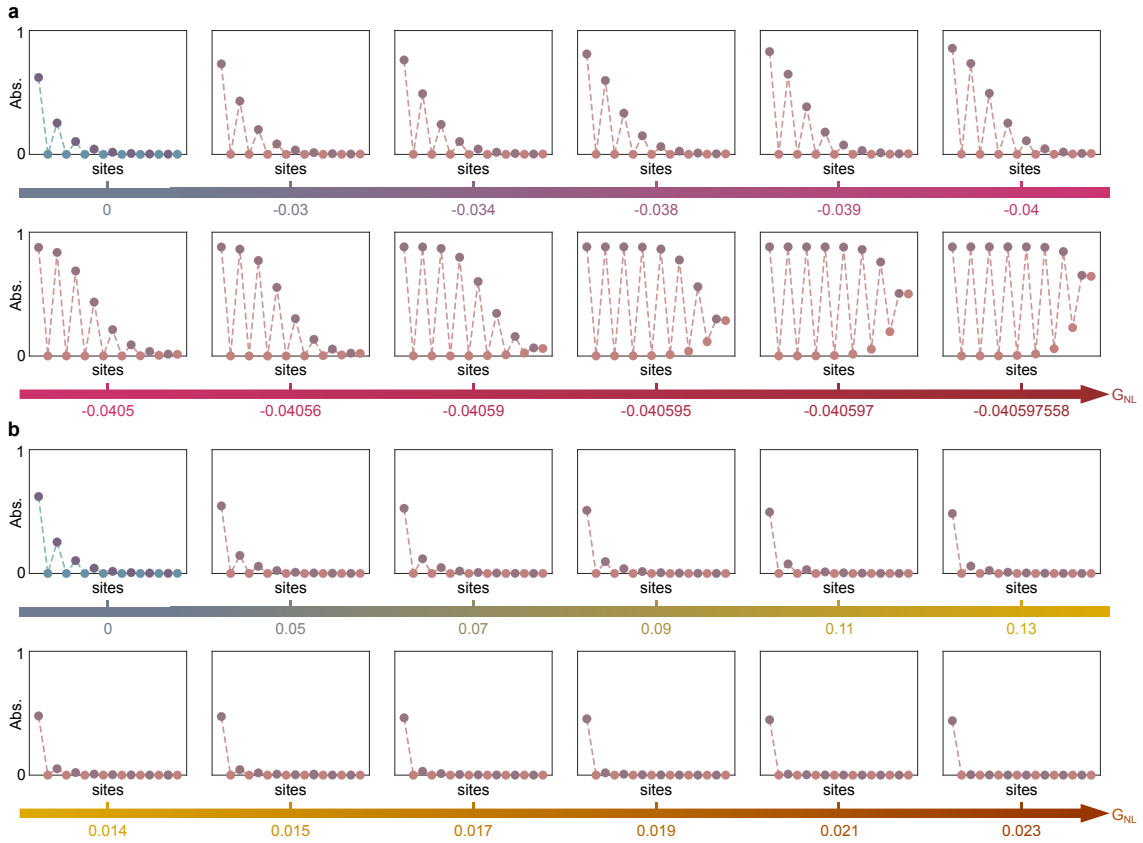
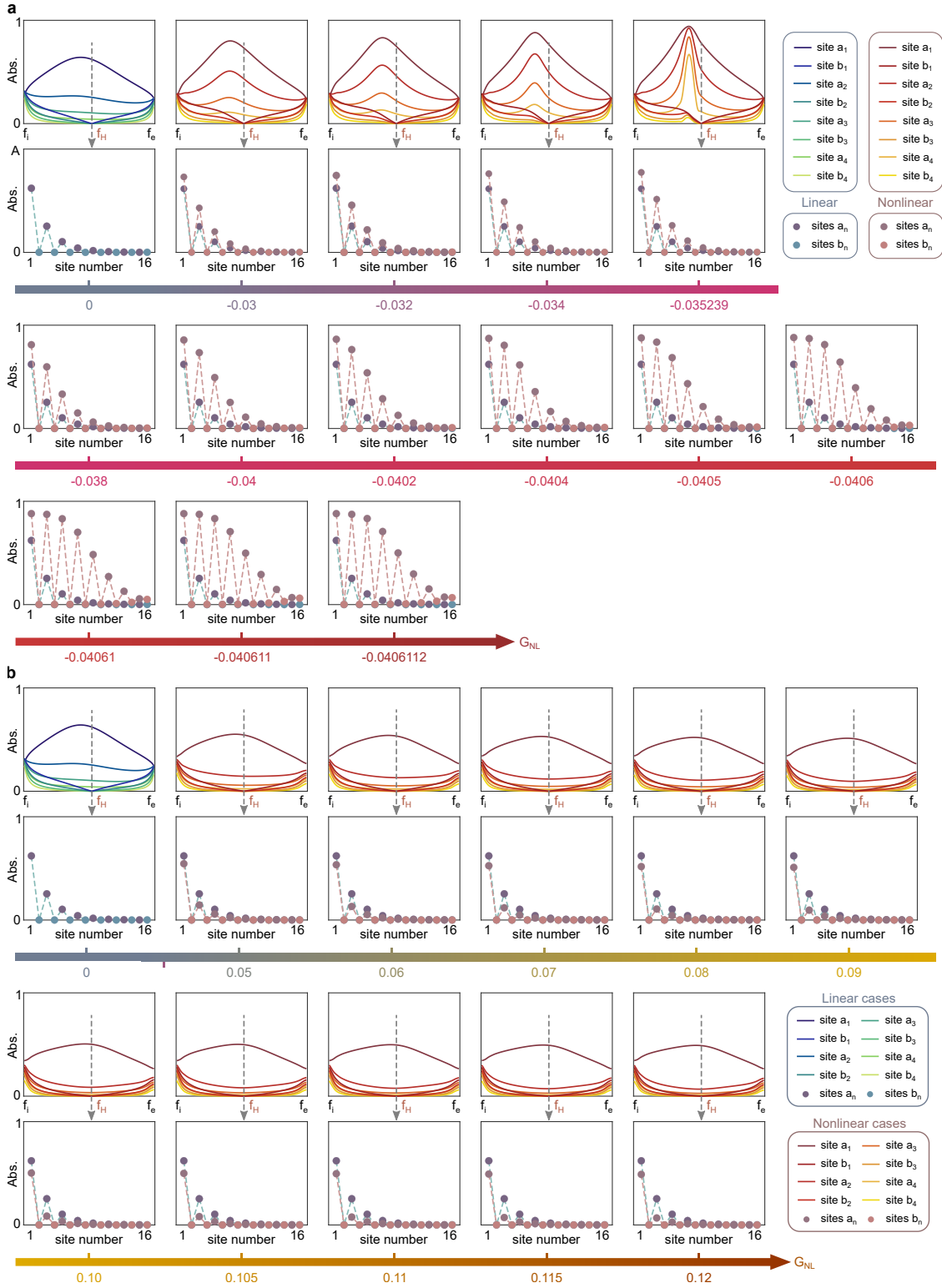


Figure 6: **Evolution of the chiral symmetry protected nonlinear topological edge states: detailed theoretical results.** The solutions are obtained with the Harmonic Balance Method (A.3). The level of nonlinearity is tuned using the constant parameter G_{NL} , the value of which varies in the negative (a) and positive (b) directions, respectively. All inset figures are displayed within the same amplitude range as in Fig.2 in the main text, while results of more nonlinear cases are showcased here.



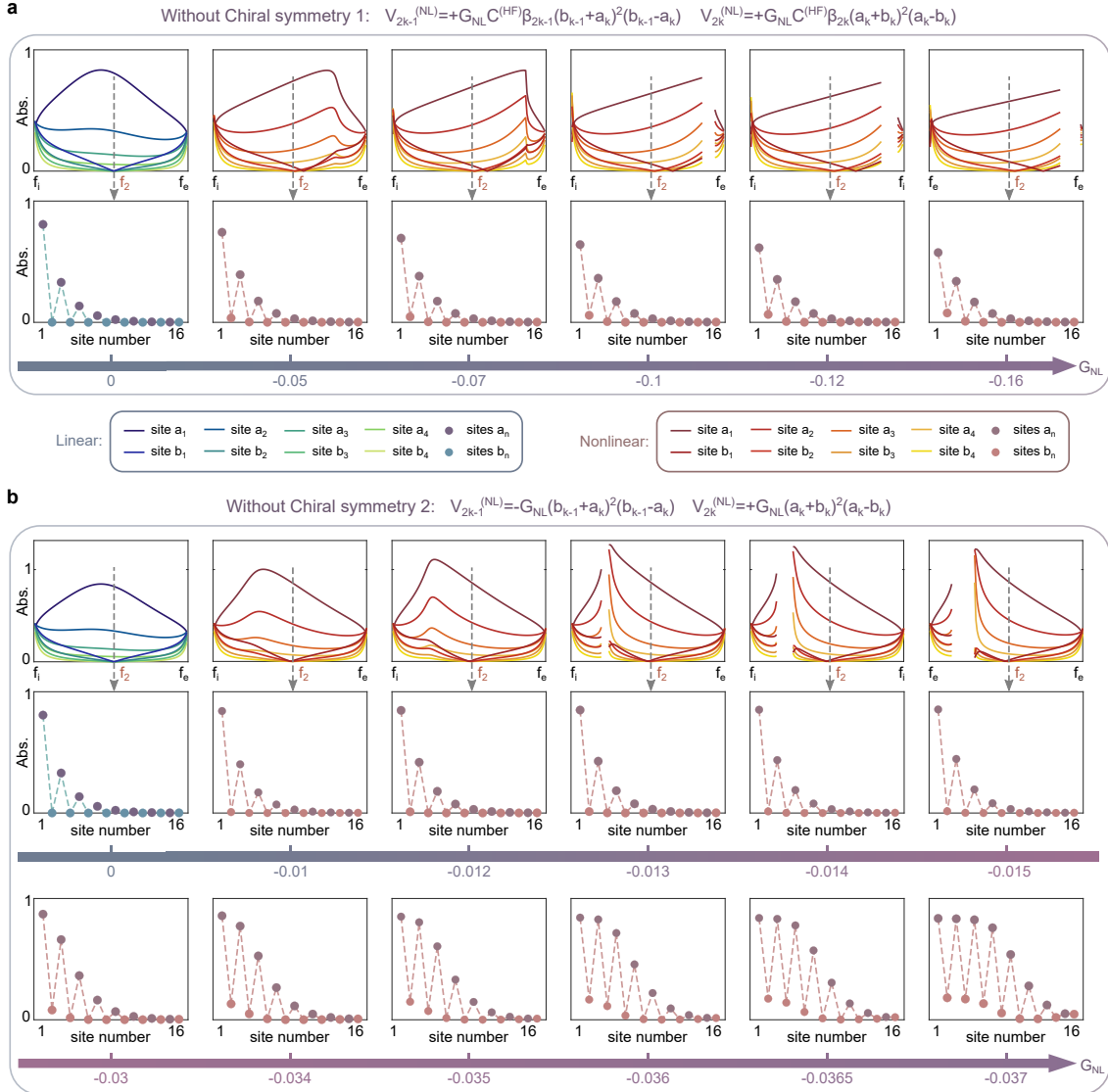
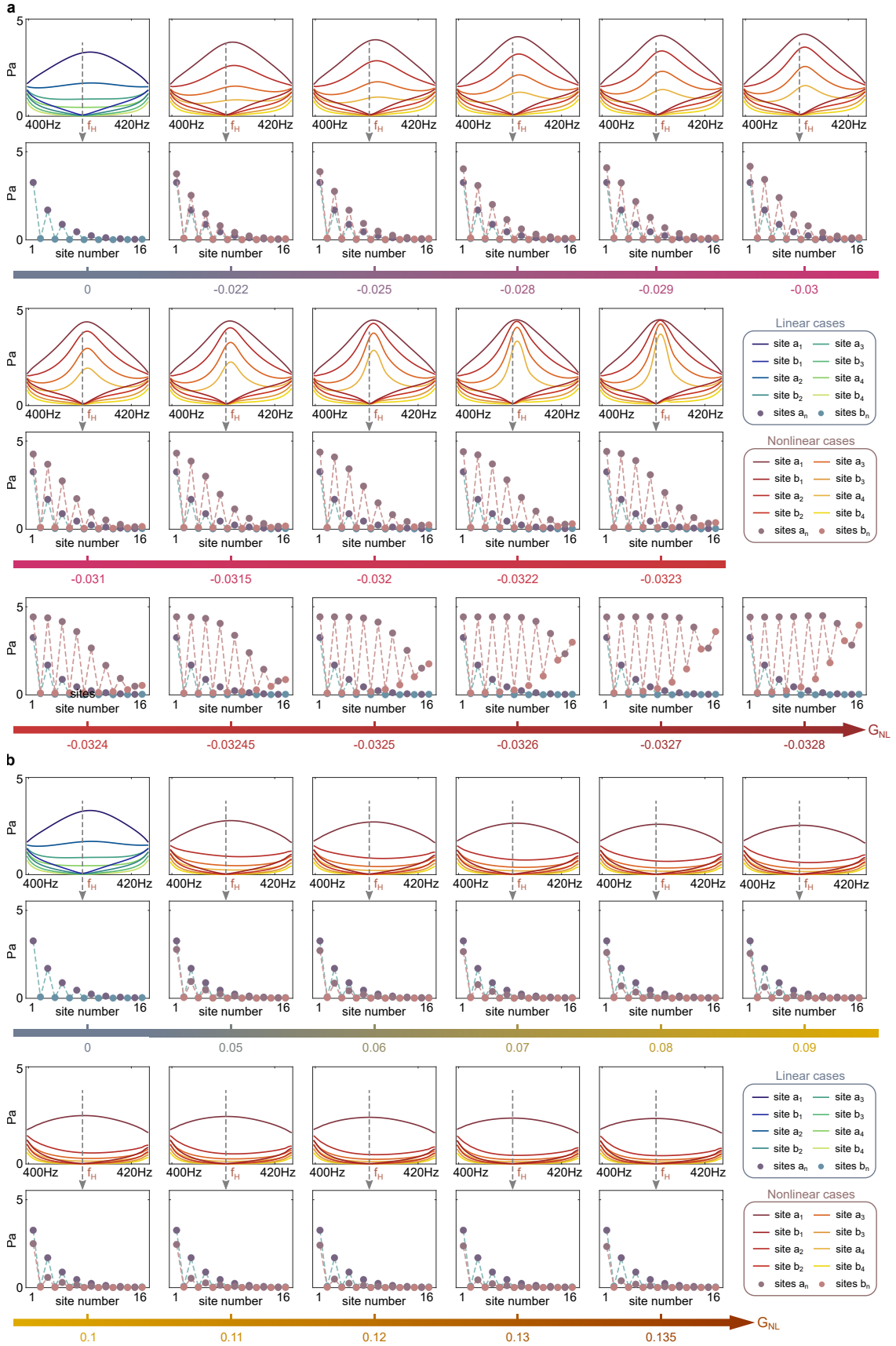


Figure 8: Evolution of nonlinear topological edge state when nonlinearities break chiral symmetry: theoretical results. Two forms of nonlinearities are investigated in (a) and (b), respectively. Results agree well with the numerical outcomes in Fig. 10 and the experimental ones in Fig. 14 where the same forms of nonlinearities are considered. They show that breaking chiral symmetry produces couplings between the two sublattices A and B, which causes the edge state to be shifted in frequency and distorted in shape.



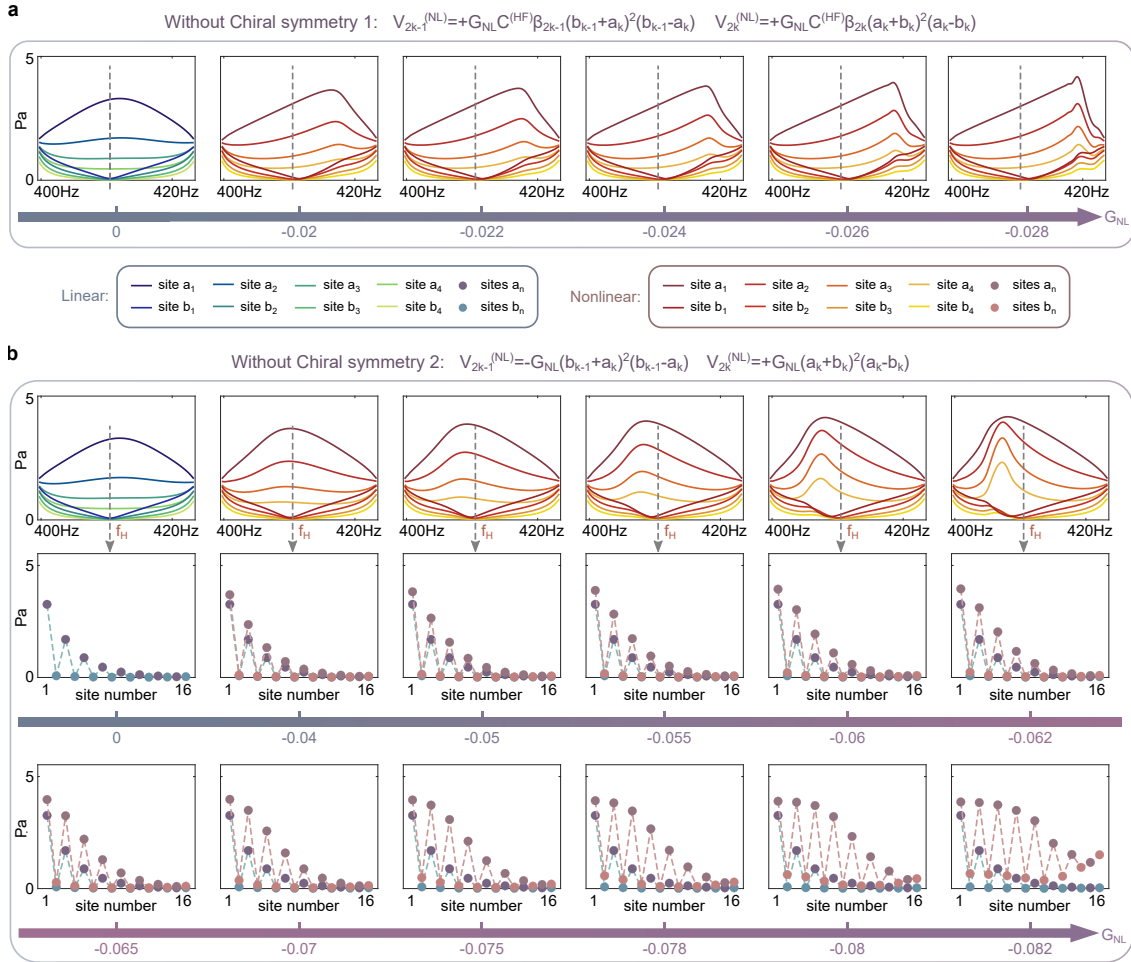


Figure 10: Evolution of nonlinear topological edge state when nonlinearities break chiral symmetry: simulation results. The actual acoustic system is simulated in the time domain. Two forms of nonlinearities are investigated in (a) and (b), respectively. Results agree well with the theoretical outcomes in Fig. 8 and the experimental ones in Fig. 14 where the same forms of nonlinearities are considered. They show that breaking chiral symmetry produces couplings between the two sublattices A and B, which causes the edge state to be shifted in frequency and distorted in shape.

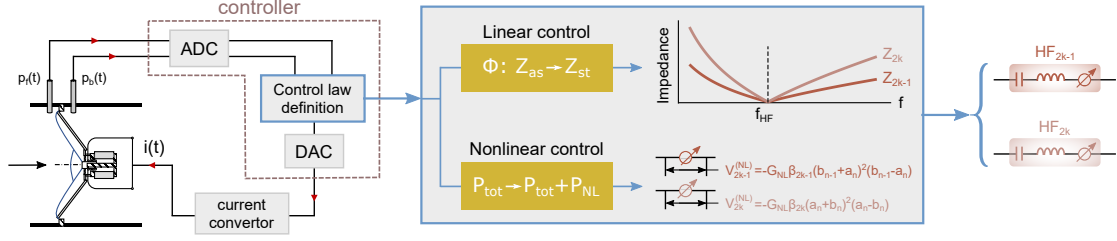


Figure 11: **Active control on the loudspeakers.** The linear part of the control is used for altering the impedance Z_n of each loudspeaker to make them resonate at the same frequency while achieving different resonance bandwidths between odd and even ones. The nonlinear part of the control is for producing the nonlinear generators $V_n^{(NL)}$ needed in the theoretical lattice in Fig. 2a. ADC (DAC) denotes the Analog-Digital (Digital-Analog) Converter. There exists a control time delay that is mainly due to the AD and DA conversions and thus unavoidable for the control law definition. We compensate for this delay effect by carefully defining the control laws, see implementation details in Appendix A.6.

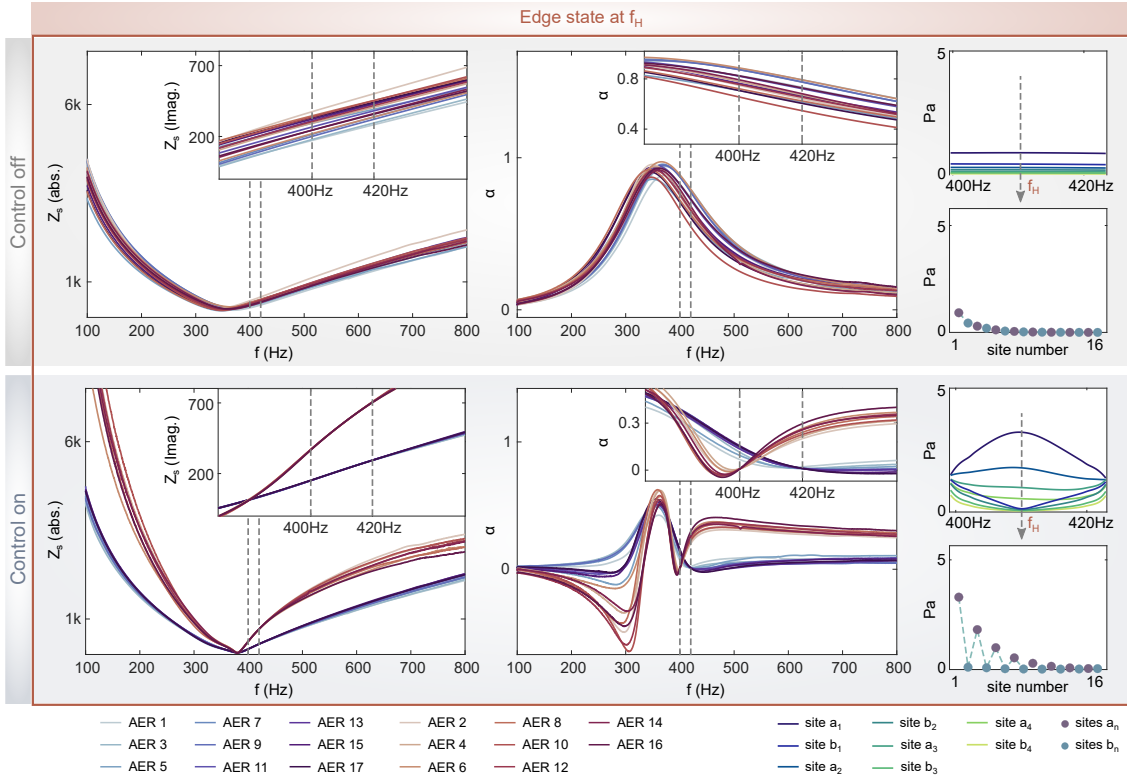


Figure 12: **Linear control results of topological edge state at f_H .** Comparison between the cases of control off and control on. The measured specific acoustic impedance Z_s and absorption coefficient α are also illustrated in both cases, for all the 17 loudspeakers in use. The edge state is linearly generated without distortions.

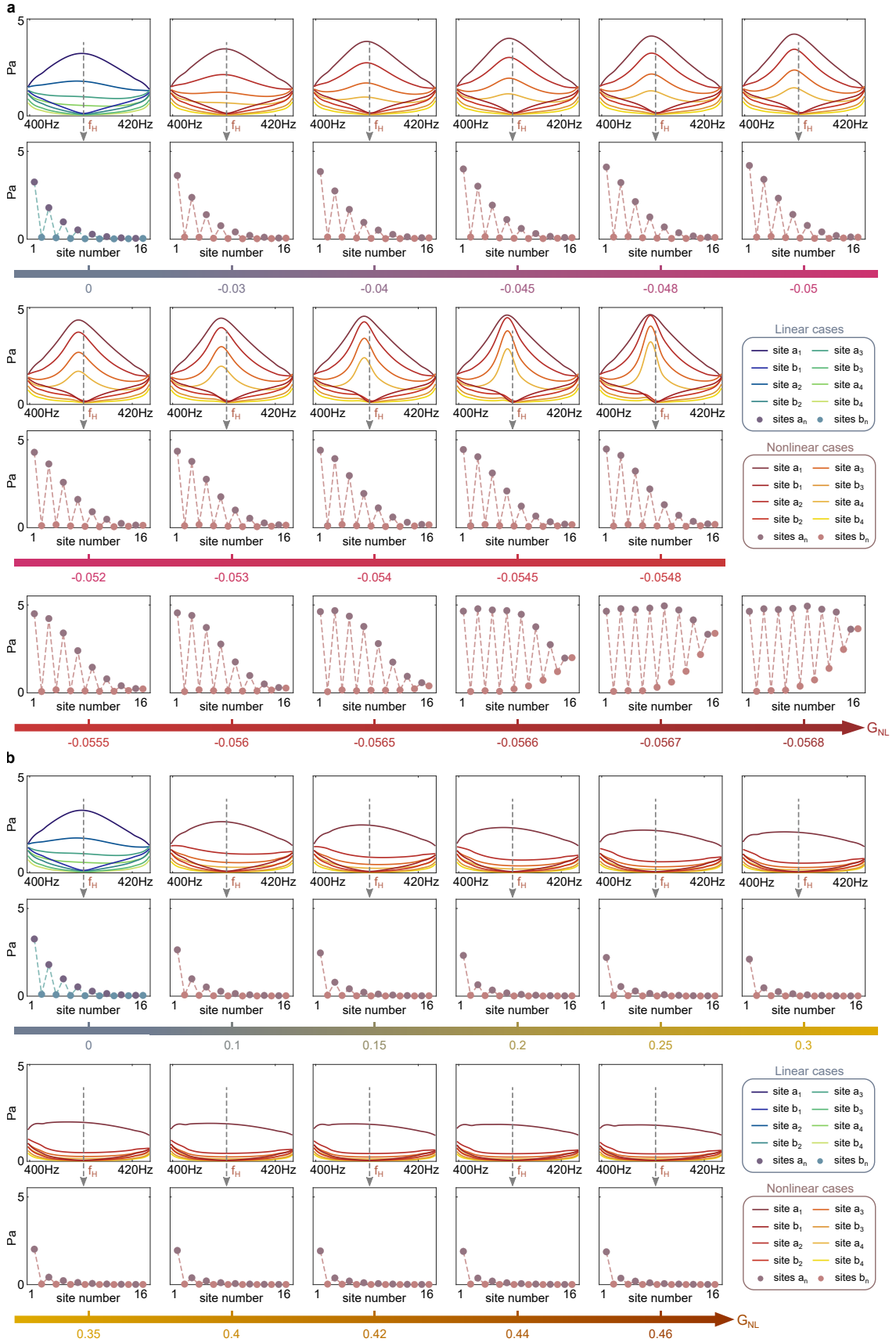


Figure 13: Evolution of the chiral symmetry protected nonlinear topological edge states: detailed experimental results. More results are given here compared to Fig. 3 in the main text, for (a) $G_{NL} < 0$ and (b) $G_{NL} > 0$, respectively.

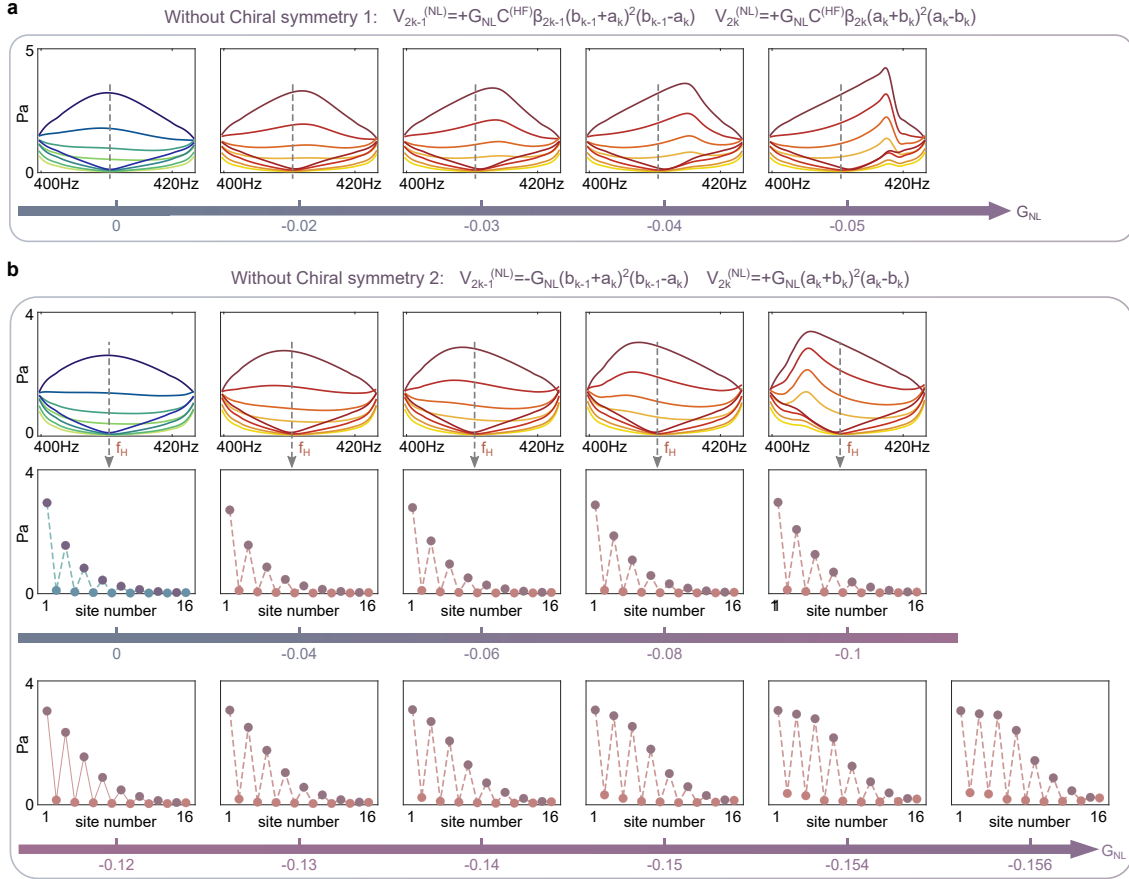


Figure 14: **Evolution of nonlinear topological edge state when nonlinearities break chiral symmetry: experimental results.** Two forms of nonlinearities are investigated in (A) and (B), respectively. Results agree well with the theoretical outcomes in Fig. 8 and the numerical ones in Fig. 10 where the same forms of nonlinearities are considered. They show that breaking chiral symmetry produces couplings between the two sublattices A and B, which causes the edge state to be shifted in frequency and distorted in shape.

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