

LEMONS: An open-source platform to generate non-circular, anthropometry-based pedestrian shapes and simulate their mechanical interactions in two dimensions

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Abstract

To model dense crowds, the usual recourse to oversimplified (circular) pedestrian shapes and contact forces shows limitations. To help modellers overcome these limitations, we propose an open-source numerical tool. It consists of an online platform with a user-friendly graphical interface to generate 2D and 3D pedestrian crowds based on anthropometric data and a C++ library that computes mechanical contacts with other agents and with obstacles, and evolves the crowd's configuration. Both can readily be called from Python scripts and leave free reins to the user for the decisional layer of the model, i.e., the choice of the desired velocities.

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1 Introduction

1.1 Motivations

From an external physical standpoint, pedestrians are just mechanical bodies obeying Newton's equations of motion: their motion is constrained by physical interactions with the environment. They experience physical forces such as gravity and ground repulsion, which prevent sinking. Yet, they differ from inert objects in that they move autonomously without requiring external impetus. This reveals two intrinsically coupled levels of pedestrian dynamics: the mechanical level and the decision-making level. Crowd literature reflects this duality. Some studies focus on mechanical aspects (essential in high-density scenarios) [1, 2] but most often relying on idealised interaction forces and simplified circular shape that fail to replicate mechanical interactions faithfully; others examine decision-making (especially relevant in low-density contexts) [3, 4], while yet others [5] address the coupling of both levels, crucial in intermediate-density situations where individuals navigate to avoid collisions, but may nonetheless experience physical contact.

Most existing crowd dynamics models [2, 5, 7] represent pedestrians as disks. However, when using the bideltoid breadth (defined in Fig. 2) as the disk diameter, a tightly packed random arrangement of a realistic population (shown in Fig. 1) only achieves densities of about 4 ped/m^2 . This falls far short of empirically observed peak densities, which sometimes exceed 8 ped/m^2 in real-world scenarios [8–10]. A potential solution to reconcile this density discrepancy would be to reduce disk diameters to the chest depth (instead of the bideltoid breadth). However, this adjustment introduces critical flaws. First, it preserves the unrealistic circular body geometry, which fails to reflect human morphology and limits the number of simultaneous physical contacts by pedestrian to six, at most. In contrast, in controlled dense crowd scenarios [11, 12], single individuals experiencing simultaneous contact with eight distinct others were observed. Second, narrower disks would artificially lift constraints on unidirectional flow in narrow corridors and overestimate the associated flow rate. Therefore, we turn to an alternative solution, using elongated shapes to represent the mechanical shape of a pedestrian.

The use of anisotropic shapes in the granular materials literature is well-established. Discrete element simulations have employed diverse geometries to describe solid dynamics: el-

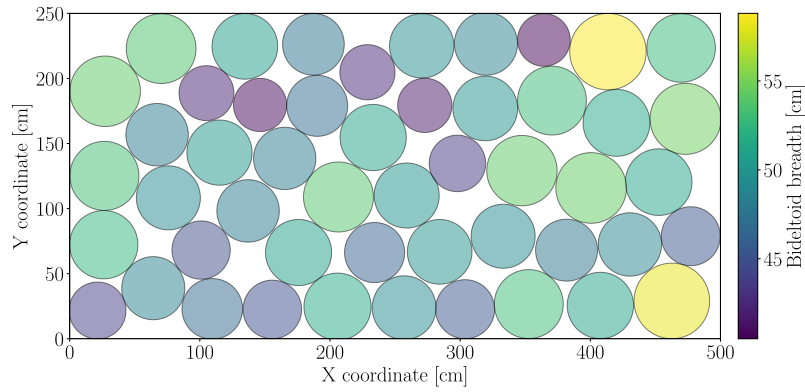


Figure 1: Tightly packed random pedestrian disk arrangement, reaching a density of 4 ped/m^2 . The disk diameters are sampled from the empirical bideltoid breadth distribution of a US population subset (ANSURII database, [6]), with mean 49 cm and standard deviation 4 cm. Algorithm details: App. D.

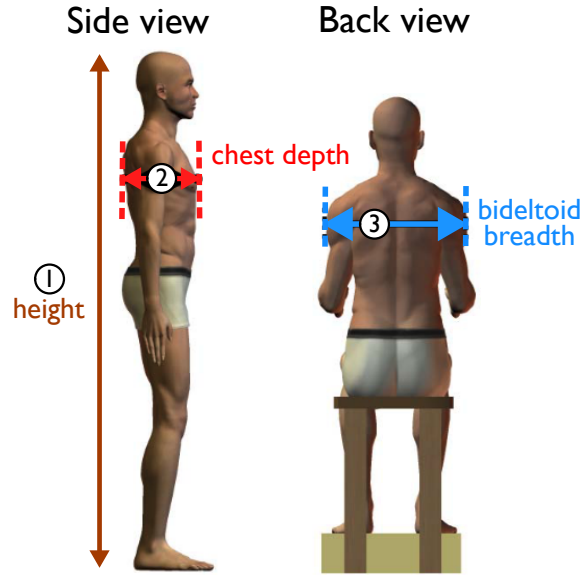


Figure 2: Illustration of anthropometric measurements – including height, chest depth and bideltoid breadth – adapted from [6].

61 lipses [13], polygons [14], polar-form polygons [15], and disk assemblies [16] represent key
 62 examples, while [17] provides a comprehensive review. Despite extensive research on granu-
 63 lar dynamics, pedestrian models rarely integrate non-circular shapes within mechanical frame-
 64 works. Still, a number of exceptions are noteworthy. Elliptical volume exclusion was incor-
 65 porated into generalised centrifugal force models, prioritising inertial forces over traditional
 66 damped-spring mechanics for pedestrian contact [18]. For models relying on the concept of
 67 velocity obstacles, the original circular agents' shapes were gradually extended to ellipsoids
 68 (EORCA), or polygonal approximations thereof for computational efficiency [19, 20], and to
 69 arbitrary shapes approximated by stitching rounded trapezoids centered on the medial axis of
 70 the shape [21]. These ellipsoidal or arbitrarily-shaped representations govern the choice of
 71 an optimal velocity that ideally enables collision-free navigation (decisional purpose), alien
 72 to any consideration of mechanical interactions. If one focuses on models including short-
 73 range and/or contact interactions, Langston et al. represented pedestrians with three overlap-
 74 ping circles in a discrete-element simulation [22], while spheropolygons [23] or spherocylin-

ders [24, 25] were later introduced in force-based simulations incorporating self-propulsion forces as well as granular material interactions governed by Newtonian mechanics, notably to model competitive egress scenarios. Recently, the human torso has been modelled as a capsule in a flow governed by position-based dynamics, supplemented with short-range interactions [26].

Nevertheless, albeit anisotropic, these shapes face significant limitations: they are more or less arbitrarily defined and lack a quantitative medical or anthropometric basis. Consequently, the generated crowds lack representative heterogeneity, which is crucial for accurately replicating density and collision statistics. These rigid structures also resist extension to new contact models involving deformation or relative motion between the centres of mass of the body segments. This article addresses these limitations by introducing a tool that generates realistic crowds from anthropometric data, simulates mechanical interactions, and allows user-defined decisional layers. It therefore removes the technical barriers of modelling elongated crowd shapes, allowing the community to focus on decision-making and its interaction with mechanics. This tool also opens the door to exploring essential questions about introducing complexity into modelling, such as whether to introduce a third dimension or incorporate heterogeneity in agent types, like strollers or individuals carrying bags.

In addition to serving researchers in the field, this tool is designed for crowd modellers at all levels, starting from beginners, in their efforts to assist, e.g. public authorities and businesses; it provides them with the possibility to achieve more realistic simulations of dense (and possibly heterogeneous) crowds in a simple way. In this particular regard, existing simulation software, such as Iventis [27] and Vadere [28], fail to reflect the latest advances; our solution brings crowd simulation into the present.

Finally, the proposed tool, dubbed LEMONS, may also be of pedagogical interest. It can easily be integrated into classroom settings, enabling teachers and science communicators to simulate agents with minimal effort. It has the potential to spark interest in the physical sciences, particularly in the study of complex systems and active matter.

1.2 How to read this document

This document exposes the theoretical foundations of the LEMONS software tool and provides an overview of the code structure. A minimal usage example, detailed usage tutorials (along with Jupyter Notebooks), and a comprehensive API documentation of the classes and functions in LEMONS can be found online [29]. Great care has been taken in the development of the codebase to make it user-friendly, easy to expand, and maintainable, as detailed in App. E.

This article is structured as follows. We begin by outlining the theoretical foundations of the project, introducing a novel mechanical shape for pedestrians, describing the generation of realistic crowds based on anthropometric data. Sec. 2.2 also details the specification of mechanical interactions between agents' shapes and with any walls present in the environment. The document then provides an overview of the code structure in Sec. 3. Finally, in Sec. 4, we present an in-depth discussion of our model, outline the tests conducted to validate its implementation, and propose potential directions for future improvements. We also provide detailed instructions on how to run a crowd evacuation simulation in this section. Supplemental videos of the tests and of the practical case studied are also provided [30].

2 Theory & Methods

2.1 From the individual pedestrian's shape to the generation of a synthetic crowd

For realistic pedestrian shapes, we relied on medical data, specifically, cross-sectional images from two cryopreserved middle-aged cadavers (a male at 1 mm intervals and a female at 0.33 mm intervals) provided by the [Visible Human Project](#) [31]. Since simulations in 2D prevail in the field of pedestrian dynamics, we need to project the 3D shape onto a suitable effective 2D shape. To this end, we selected the cross-section at torso height, an example of which is shown in Fig. 3 for the male specimen; this choice is notably justified by the fact fatalities during crowd crushes often result from asphyxia and severe compression of the rib cage and lungs. We approximated the torso slice with a set of five partly overlapping disks: two for the shoulders, two for the pectoral muscles, and one for the back, as illustrated in Fig. 7. Disks were chosen over polygons because defining and computing mechanical contact between disks is much simpler and more computationally efficient [17].

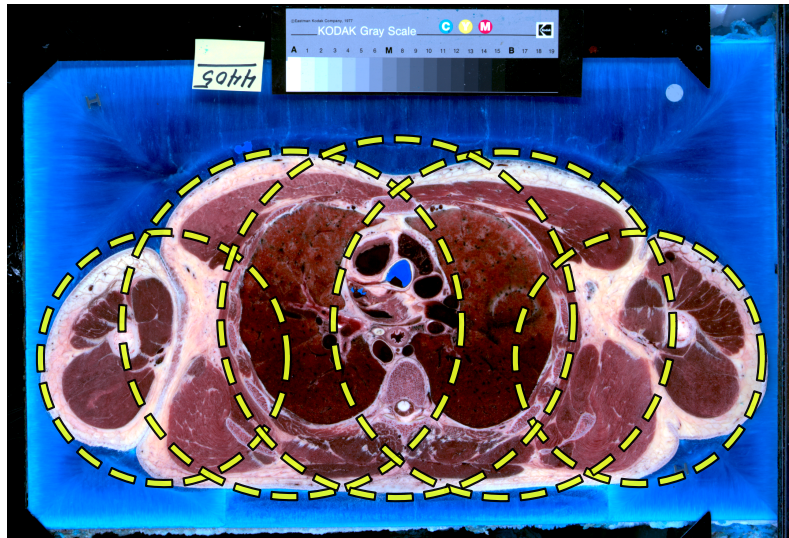


Figure 3: Torso section of a cryopreserved man, slice number 4405, from the [31] database, covered with five disks. The ‘Kodak Q-13 Gray Scale’ ruler measures 20.3 cm by 2.5 cm.

To extend the fitting method to a whole population, we utilised anthropometric data from the [ANSURII](#) database [6], which comprises 93 body measurements from 6,000 [US](#) Army personnel (4,082 men and 1,918 women). In the Anthropometry tab of our online app, these data are easily accessible, viewable, and downloadable. Note, however, that this sample is not fully representative of the [US](#) civilian population; in particular, among other selection biases, men are over-represented, whereas women form the majority of the [US](#) population, according to the [NHANES](#) database [32]¹ (which can be partly explained by the higher life expectancy of women in the [US](#) population). To generate a crowd that reflects the anthropometric diversity of [ANSURII](#) starting from the foregoing 2D projection made of five disks, we translate the centres of the disks with a homothety centred at the pedestrian’s centre of mass and scale their radii to match empirical chest depth and bideltoid breadth measurements (defined in Fig. 2). These geometric operations do not perfectly preserve the initial shape, but they achieve a real-

¹[NHANES](#) provides only limited measurements and lacks key metrics such as bideltoid breadth and chest depth and therefore cannot be used in our software.

istic approximation. Compared to the maximal possible density around 4 ped/m² for circular agents (see Fig. 1), crowds generated with these methods can reach a density of 7.2 ped/m² (see Fig. 4), much closer to empirical measurements in very dense situations [8–10].

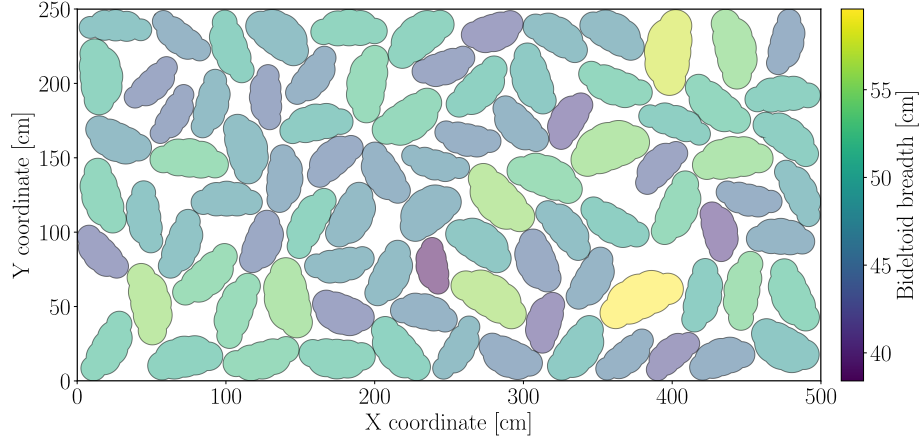


Figure 4: Tight random packing of pedestrians without preferred orientation using an arrangement of five disks, reaching a density of 7.2 ped/m². Both the sample from the *ANSURII* database [6] and our model database have a mean bideltoid breadth of 49 cm and a mean chest depth of 25 cm.

2.2 Mechanical interactions

Studying the mechanical interactions between pedestrians presents inherent complexity, arising from factors such as three-dimensional contact geometry, protective hand movements during contacts or falls, and non-static multi-point contacts [12, 33]. Even though bio-mechanical studies have characterized stress-strain relationships in fresh, non-rigid cadavers subjected to dynamic loading — both frontal [34, 35] and lateral [36] — and have measured contact forces among pedestrians under varying degrees of crowding, in both static and dynamic conditions [37], the fundamental nature of live pedestrian-to-pedestrian contact remains poorly understood. This is especially true during complex, multi-body collisions, where active interventions, such as the use of hands, may significantly influence the interaction dynamics. To make the problem tractable, we deliberately simplify these interactions by relying on granular material interactions between the disks that constitute each agent’s shape. Specifically, we model the interaction in the simplest way we find appropriate, using a single-damped spring as illustrated in Fig. 5. The stick-and-slip process at a dynamic contact follows Coulomb’s law. Another force is introduced to encompass the effective backwards friction with the ground over a step cycle, controlled by the deformation of the body. Technical details are given in App. A.1, and a comprehensive overview of notations, definitions, and mathematical expressions can be found in App. A.3.

Finally, the deliberate forward motion is subsumed into a propulsion force \mathbf{F}_p for translational motion (and a propulsion torque τ_p for deliberate rotations of the torso) which result from the pedestrian’s decision-making process. The LEMONS platform is agnostic to the decision-making model: it leaves free reins to the user to define \mathbf{F}_p and τ_p for each agent as they see fit (see Eq. 4 for a crude proposal). The equation of motion of the centre of mass of agent i (mass m_i , translational velocity \mathbf{v}_i) is then expressed as:

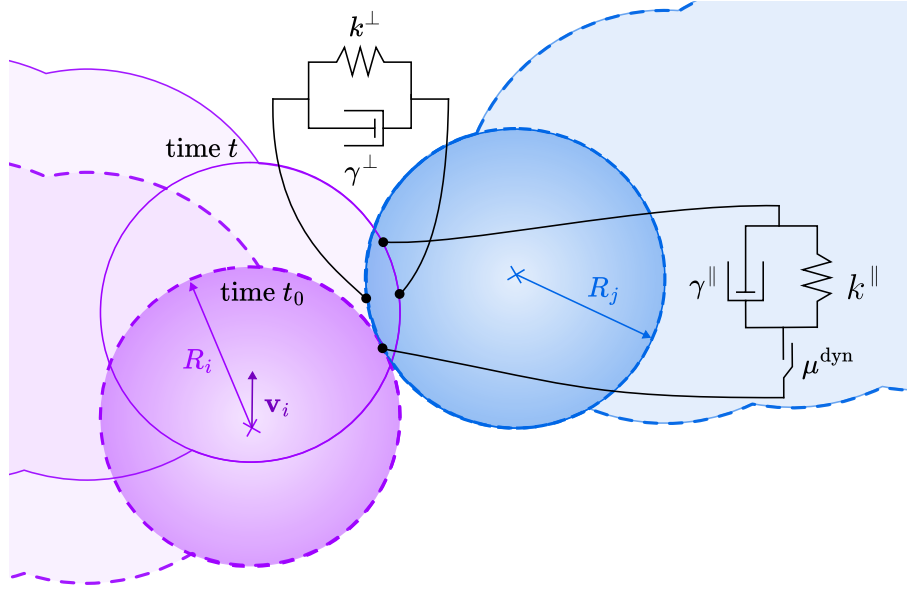


Figure 5: Interactions between composite disks of pedestrians i (radius R_i , velocity \mathbf{v}_i) and j (radius R_j , stationary with $\mathbf{v}_j = \mathbf{0}$) are modeled using mechanical elements. In the normal direction (orthogonal to the contact surface), the interaction is described by a spring in parallel with a dashpot (Kelvin–Voigt model), which captures both elastic effects and energy dissipation. In the tangential direction (parallel to the contact surface), the interaction is modelled by a parallel spring-dashpot system in series with a slider, reflecting Coulomb’s law. This slider represents a threshold-based element that resists tangential motion until a critical force threshold, proportional to the normal force, is exceeded; after this threshold is reached, it slips at a constant force. The dashed line indicates the pedestrian shape at the onset of contact.

$$m_i \frac{d\mathbf{v}_i}{dt} = \mathbf{F}_p - m_i \frac{\mathbf{v}_i}{t^{(\text{transl})}} + \sum_{(s^{(i)}, s^{(j)}) \in \mathcal{C}_i^{(\text{ped})}} \left(\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\parallel \text{contact}} + \mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} \right) + \sum_{(s^{(i)}, w) \in \mathcal{C}_i^{(\text{wall})}} \left(\mathbf{F}_{w \rightarrow s^{(i)}}^{\parallel \text{contact}} + \mathbf{F}_{w \rightarrow s^{(i)}}^{\perp \text{contact}} \right) \quad (1)$$

170 where

$$\begin{aligned} \mathcal{C}_i^{(\text{ped})} &= \{(s^{(i)}, s^{(j)}) \mid s^{(j)} \text{ in contact with } s^{(i)}\}, \\ \mathcal{C}_i^{(\text{wall})} &= \{(s^{(i)}, w) \mid w \text{ in contact with } s^{(i)}\}. \end{aligned} \quad (2)$$

171 Here, $t^{(\text{transl})}$ is a characteristic timescale for the effective backwards friction and the $s^{(i)}$ repre-
 172 sents the five disks that form agent i . The symbol \parallel indicates a force tangential to the contact
 173 surface, while \perp signifies a force orthogonal to the contact surface. These forces are applied
 174 to the contact centres, so that they can induce torques on the torso. The rotational dynamics
 175 of agent i ’s torso (moment of inertia I_i , angular velocity ω_i) are governed by:

$$I_i \frac{d\omega_i}{dt} = \tau_p - I_i \frac{\omega_i}{t^{(\text{rot})}} + \sum_{(s^{(j)}, s^{(i)}) \in \mathcal{C}_i^{(\text{ped})}} \tau_{G_i, s^{(j)} \rightarrow s^{(i)}} + \sum_{(s^{(j)}, s^{(i)}) \in \mathcal{C}_i^{(\text{wall})}} \tau_{G_i, w \rightarrow s^{(i)}} \quad (3)$$

where $t^{(\text{rot})}$ is a characteristic timescale for rotational damping and the $\tau_{G_i, s^{(j)} \rightarrow s^{(i)}}$ refer to the torque at the centre of mass G_i of pedestrian i , resulting from pedestrian-pedestrian interaction forces. A (very) crude choice for the propulsion force and torque is

$$\mathbf{F}_p = m_i \frac{v^{(0)} \mathbf{e}^{(\text{target})}}{t^{(\text{transl})}} \quad \text{and} \quad \tau_p = I_i \frac{-\delta\theta}{(t^{(\text{rot})})^2}, \quad (4)$$

where $v^{(0)}$, $\mathbf{e}^{(\text{target})}$, and $\delta\theta$ are the preferential speed, the unit vector pointing to the target (or way-point), and the angular mismatch between the target direction $\mathbf{e}^{(\text{target})}$ and the front direction of the body of agent i . To solve this set of coupled differential equations of motion, we employed the standard Velocity-Verlet algorithm mentioned in [38], section 3. For additional information on the determination of neighbours, please refer to App. B.

3 The Codebase

The software release consists of (i) an online platform <https://lemons.streamlit.app/> to generate and visualise individual pedestrians (whose shapes are compatible with anthropometric data) or crowds, (ii) a C++ library to compute mechanical contact forces in two dimensions and then evolve the crowd according to Newton's equation of motion, and (iii) a Python interface to import anthropometric data, generate and visualise crowds, and simulate their dynamics via simple calls to the C++ library. It introduces a generic format for configuration files (which can be saved as XML files) to store agents' shapes and mechanical properties as well as crowds' configurations.

3.1 XML crowd configuration classes

Several levels of detail must be specified to define the configuration of a (presently 2D) crowd, from the geometric and mechanical properties of each of its agents to their positions. We introduce a generic structure made of nested classes, stored as XML files (processed by the third-party library TinyXML-2), included in the codebase, to mimic these levels of information; we hope that this structure will be used broadly for the definition of crowd configurations. To illustrate how generic it is, alongside standard adult pedestrians, we will also instantiate geometric objects corresponding to cyclists on their bikes.

Fig. 6 shows how the XML configuration files are used as input and output of the C++ library (which has a Python interface) to simulate the dynamic evolution of the crowd. The contents of each XML configuration file are detailed below. All units are expressed in the International System (SI). One example of each file (used for the practical case example presented in Sec. 4.3) is provided in App. C. We begin with the `Parameters.xml` file:

- **Parameters:**
 - ★ Directory in which STATIC files are stored,
 - ★ Directory in which DYNAMIC files are stored,
 - ★ Time step `TimeStepMechanical` of the Velocity-Verlet algorithm used to solve the dynamics,
 - ★ Duration `TimeStep` of one decisional loop, after which \mathbf{F}_p and τ_p can change, typically a fraction of a second.
- “STATIC” files contain information that does not change throughout a simulation, namely:
- **Geometry:**
 - ★ Dimensions of the simulation area,
 - ★ List of ‘obstacles’ (notably, wall), defined as ordered lists of corners (i.e., the vertices that are connected by the zero-width wall faces). Each obstacle is made of a given material, whose ID must be specified.

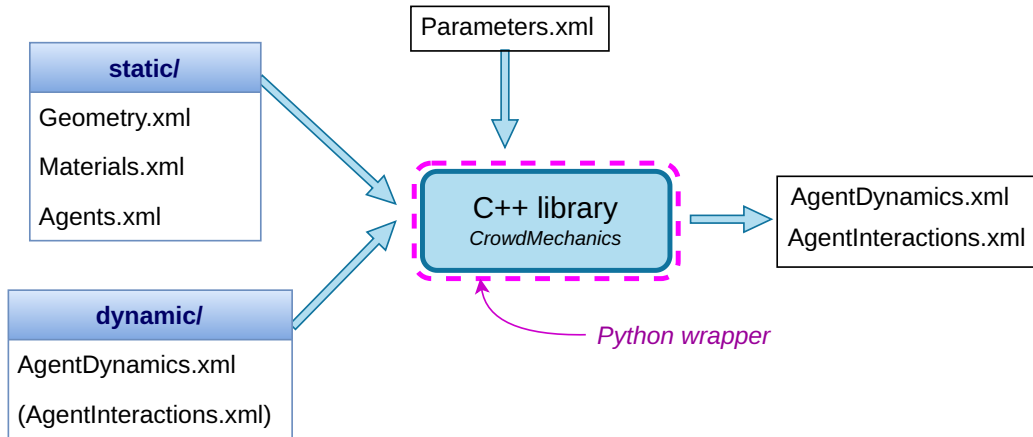


Figure 6: Functional diagram showing the XML configuration files defining the crowd and used as input and output of the mechanical simulation routine, coded in C++ and interfaced with Python.

- **Materials** (for obstacles as well as agents):
 - ★ **Intrinsic properties:** Young’s modulus E , shear modulus G relative to a unique material ID.
 - Note: these are used to calculate the spring constants for the contacts between all materials via the following formulas (derived from [39], also see Fig. 5):

$$k^{\perp} = \left(\frac{4G_1 - E_1}{4G_1^2} + \frac{4G_2 - E_2}{4G_2^2} \right)^{-1}, \quad (5)$$

$$k^{\parallel} = \left(\frac{6G_1 - E_1}{8G_1^2} + \frac{6G_2 - E_2}{8G_2^2} \right)^{-1}, \quad (6)$$

- ★ **Binary physical properties** that are not reducible to intrinsic ones: damping coefficient γ^{\perp} perpendicular to the contact surface, damping coefficient γ^{\parallel} tangential to the contact surface, dynamic friction coefficient during slip μ^{dyn} . These need to be defined for all pairs of materials.
 - **Agents:**
 - ★ ID of the agent,
 - ★ Mass,
 - ★ Height,
 - ★ Moment of inertia,
 - ★ Inverse timescale for translational friction $1/t^{(\text{translational})}$ (FloorDamping),
 - ★ Inverse timescale for rotational damping $1/t^{(\text{rotational})}$ (AngularDamping),
 - ★ Constitutive shapes (5 for a pedestrian):
 - ▷ ID of the constitutive material,
 - ▷ Radius,
 - ▷ Initial position relative to agent’s centre of mass.
- Note: the composite shapes order is important, because the body’s orientation will be determined based on the first and last composite shapes. For a pedestrian, the first composite shape should be the left shoulder, and the last one should be the right shoulder.

“DYNAMIC FILES” are used both as input and output of the C++ library, and they contain information that changes during the execution of the code, namely:

- **AgentDynamics** (current state of the agents):

- ★ **Kinematic** quantities for each agent:

- ▷ Position \mathbf{r} of the center of mass,
 - ▷ Velocity \mathbf{v} of the center of mass,
 - ▷ Orientation (Theta) of the body concerning the x-axis, that is, the angle θ between the gaze of the agent when looking straight ahead, and the x-axis (see Fig. 11c),
 - ▷ Angular velocity (Ω).

- ★ **Dynamic** quantities for each agent (not written in the output files):

- ▷ Propulsion force \mathbf{F}_p (F_p),
 - ▷ Driving torque for the torso τ_p (M_p).

Note: all angular quantities are given relative to the z-axis, with the trigonometric convention.

- **AgentInteractions:**

- ★ Normal force $\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}}$ (F_n), tangential force $\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\parallel \text{contact}}$ (F_t), and tangential spring elongation (`TangentialRelativeDisplacement`) also known as slip (see Sec. A.1.1) between all pairs of composite shapes in contact (that do not belong to the same agent),
 - ★ Normal force $\mathbf{F}_{w \rightarrow s^{(i)}}^{\perp \text{contact}}$, tangential force $\mathbf{F}_{w \rightarrow s^{(i)}}^{\parallel \text{contact}}$, and slip between all pairs (wall – composite shape) in contact.

Note 1: using the symmetries of forces and spring elongation, we only list the values once for each pair (composite shape – composite shape or wall – composite shape) in contact.

Note 2: this file is only provided if there are contacts between agents or between agents and walls. No such file is needed in the initial configuration, provided there are no overlaps; for the following runs, the output file can be used *unchanged* for the next run.

3.2 Mechanical layer

In Fig. 6, the mechanical layer *CrowdMechanics* is a C++ shared library that handles the dynamics of the agents described in Sec. 2.2. Calling instructions from C++ and Python are provided in the online tutorials [29].

3.3 Python classes

The Python wrapper mirrors the foregoing structure, insofar as it contains Python classes corresponding to the foregoing XML configuration files. However, since it also allows for generating a synthetic crowd based on anthropometric statistics and visualising it in 2D and in 3D, additional Python classes needed to be defined. The following classes and ‘dataclasses’ (which contain the statistics and measurements relevant for the generation of the crowd or the agent) are provided:

- ★ **Crowd class:** group of *Agent* objects.

The class contains methods to generate a crowd that abides by the measurement constraints of *CrowdMeasures* and to position the agents either on a grid or using the packing algorithm detailed in App. D.

- ★ **CrowdMeasures dataclass:** Collection of dictionaries representing the characteristics. By default, it contains ANSURII-based anthropometric statistics. But the user can define custom normal distributions for each agent’s attributes (e.g., pedestrian bideltoid breadth, bike top tube length).

- ★ **Agent class:** represents a single pedestrian (or bike rider, etc.)

- 291 ★ **AgentMeasures dataclass**: Collection of attribute measurements (e.g., chest depth,
 292 mass, height for pedestrians; handlebar length, total bike weight for bikes). The at-
 293 tribute values are taken from *CrowdMeasures* if the agent is instantiated from a *Crowd*;
 294 alternatively, they can be specified manually if agents are created one by one.
- 295 ★ **InitialPedestrian class**: 2D and 3D contour shapes of a reference pedestrian.
 296 The 2D shape consists of 5 overlapping discs, whose outer contour matches that of a
 297 cryogenic specimen at shoulder's height² (see Sec. 2.1 and Fig. 3). There is one 2D tem-
 298 plate that applies to both men and women, and separate 3D templates: one for men and
 299 one for women. To further emphasise the versatility of the file structure, an **InitialBike**
 300 **class** was also defined to represent the shape of a rider on a bike, that is to say, a top-
 301 down approximate orthogonal projection of the bike and the rider.
 302 The 3D shape takes the form of a dictionary where each key corresponds to a specific alti-
 303 tude and each value is a `Shapely.MultiPolygon` object. Each `Shapely.MultiPolygon`
 304 contains multiple `Shapely.Polygon` objects, each of which is a polygon representing
 305 a distinct part of the body—such as a finger, an arm or a leg etc. This is illustrated in
 306 Fig. 7.
- 307 ★ **Shapes2D class**: 2D shape of a particular agent (pedestrian, bike, ...).
 308 The 2D pedestrian's shape is obtained by transforming the reference 2D shape (**InitialPedestrian**
 309 **class**) to match the measurements specified in **AgentMeasures**. More precisely, the radii
 310 of the five disks are uniformly rescaled to match the specified chest depth, defined by the
 311 diameter of the middle disk. Additionally, a homothety centred at the agent's centroid is
 312 applied to the centres of each of the five composite disks to match the specified bideltoid
 313 breadth.
 314 A similar process is applied for 2D bike shapes; it hinges on the application of homoth-
 315 eties to each composite shape of the reference bike.
- 316 ★ **Shapes3D class**: 3D shape of a particular agent (only for pedestrians at present).
 317 Starting from the reference pedestrian (**InitialPedestrian class**), the dimensions of each
 318 `Shapely.Polygon` at various altitudes are adjusted along with the altitude values them-
 319 selves. Specifically, a vertical homothety is applied to ensure that the resulting shape
 320 matches the desired pedestrian height. Additionally, a homothety is applied to each
 321 contour of our reference cryogenic specimen defined in the *InitialPedestrian* class; the
 322 centre of the homothety is set at the mean of the x and y coordinates of each polygon's
 323 centroid. The scaling factors s_{init} for the homothety are selected to match the chest depth
 324 and bideltoid breadth specified in *AgentMeasures*.
 325 In detail, the chest depth is defined as the maximum distance between two points along
 326 the orientation-axis of the `Shapely.MultiPolygon` (i.e., the x-axis if the agent is
 327 turned to the right, corresponding to $\theta = 0$) in the slice at torso's height (the altitude
 328 used to measure the bideltoid breadth of the cryogenically preserved specimen). The
 329 bideltoid breadth is defined as the maximum distance between two points along the axis
 330 orthogonal to the orientation-axis of the `Shapely.MultiPolygon` (the y-axis if $\theta = 0$)
 331 at the foregoing altitude.
 332 To avoid inflating the head and feet because of the homothety, the scaling factors s_{init}
 333 are modulated with the altitude z ; the final scaling factor is $s_{\text{new}}(z) = f(z, s_{\text{init}})$, where
 334 $f(z, s)$ is a smooth, door-shaped function equal to 1 for altitudes above the neck and
 335 below the knees (meaning no rescaling in those regions) and to s elsewhere. This ap-
 336 proach ensures that, unlike the head, the belly and abdominal regions are duly inflated
 337 and reflect morphological differences, particularly for bigger individuals.

²More precisely, we consider the horizontal slice at the altitude used to measure bideltoid breadth in our 186.6 cm-tall reference cryogenic male specimen; the same altitude was used to measure the bideltoid breadth of the female specimen (whose feet are extended as if she were on tiptoe, resulting in an elongated posture)

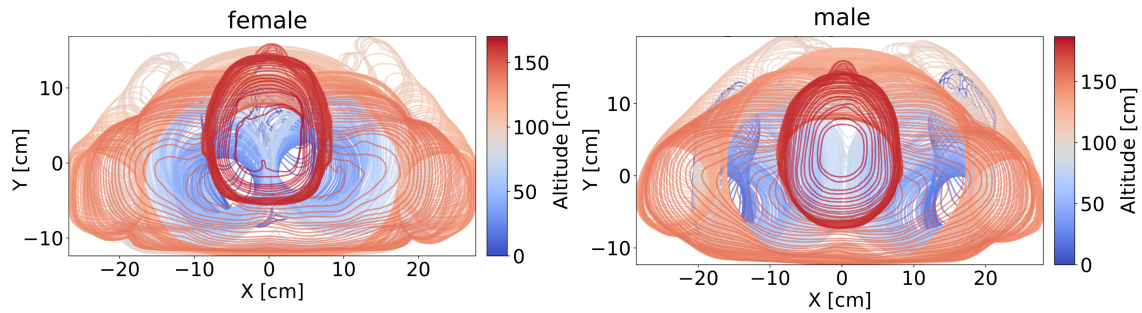


Figure 7: Superimposed cross-sectional contours from two cryogenically preserved bodies, sampled at 0.5 cm intervals. The two bodies belong to a female on the **left** and a male on the **right**. The contours were obtained by processing the images of each section from the dataset [31]. The upper body displays a reddish hue, while the lower part appears bluish.

338 4 Discussion

339 4.1 Relevance of the use of 2D projections of standing pedestrians

340 In line with the dominant approach in pedestrian dynamics, our code primarily operates on 2D
 341 shapes, although it provides access to 3D visualisation. This simplification may be questioned
 342 not only because pedestrians may raise their arms to protect their chest in very dense settings,
 343 but also because people have different heights, so that it may be inadequate to assess their
 344 contacts based on 2D projections at torso height. Shorter individuals (e.g., children, women,
 345 etc.) may have their heads at the level of the chests or shoulders of taller ones. Consequently,
 346 2D crowd representations can vary significantly depending on the viewpoint of the pedestrian;
 347 the practical impact of this question of perspectives remains unclear. Our platform enables us
 348 to gauge the extent to which 2D projections reflect the packing conditions in a 3D crowd
 349 composed of adults of diverse heights. For this purpose, we generate a static 3D synthetic
 350 crowd based on the **ANSURII** database. In this example, pedestrian heights range from 155 cm
 351 to 178 cm for females and from 163 cm to 201 cm for males, with a mean height of 170 cm. As
 352 shown in Fig. 8, we present a comparison between the 2D projection of the scene—constructed
 353 from our pedestrian shape models—with cross-sections extracted from the corresponding 3D
 354 crowd at three distinct altitudes: the torso height of the smallest agent, the torso height of the
 355 tallest agent, and the mean torso height across the group. These comparisons reveal that the
 356 perceived density can vary considerably depending on the pedestrian’s height. Notably, the
 357 area covered at the mean torso height is closely matched by our 2D projection approach.

358 4.2 Mechanical tests

359 Regarding agent generation, the Pytest files thoroughly test all essential functions, including
 360 rotation operations, backup file handling, and file downloading processes. They also ensure
 361 that the generated agents’ statistical properties—such as mean bideltoid breadth, mean chest
 362 depth, and standard deviation—accurately match the intended crowd statistics and anthropo-
 363 metric targets.

364 Regarding the simulation engine, a series of eight distinct tests (covering distinct scenarios)
 365 has been created. You should run these tests each time you modify the C++ code by following
 366 the steps below:

- 367 1. Navigate to the `tests/mechanical_layer` directory.
- 368 2. Run the following command in your terminal:

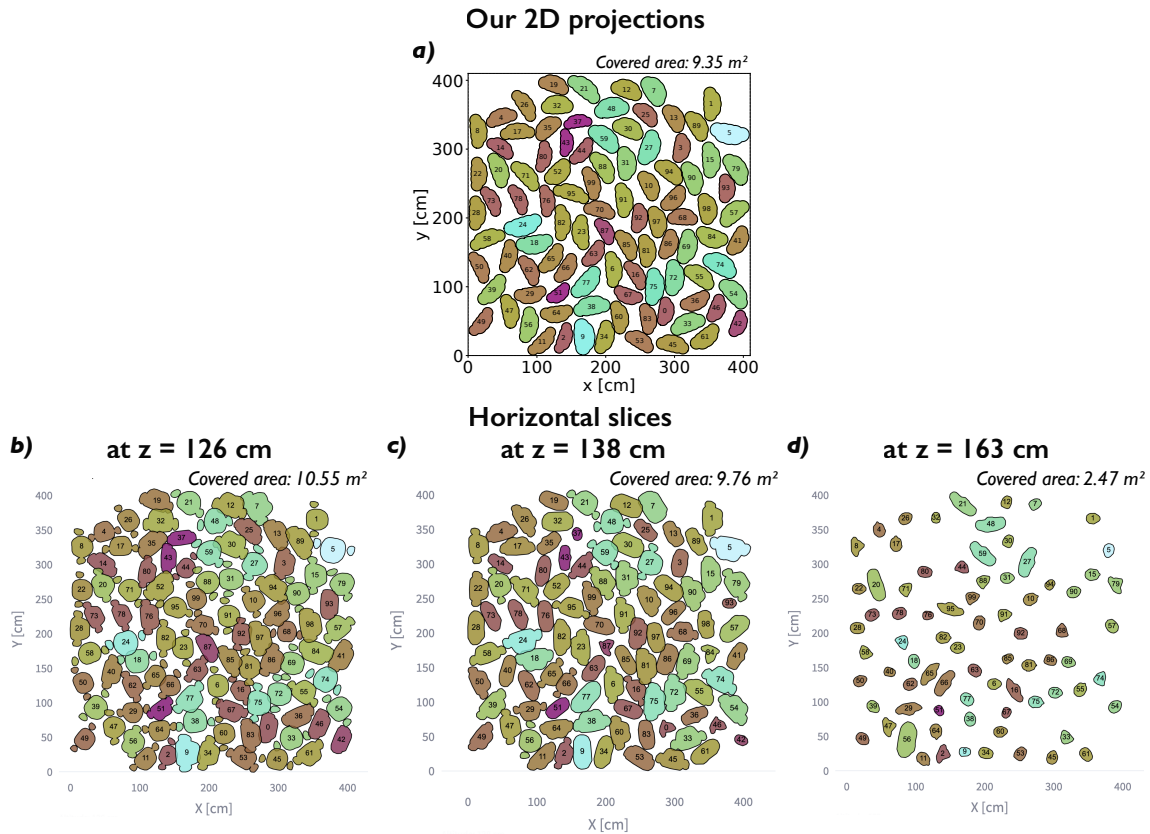


Figure 8: 2D representations of a pedestrian crowd at a density of about 6 ped/m^2 . Panel (a) shows the 2D projections that we use for the mechanical simulations, while panels (b), (c), and (d) display horizontal cross-section of the 3D crowd at altitudes $z = 126 \text{ cm}$ (the torso altitude of the smallest pedestrian in the crowd), $z = 138 \text{ cm}$ (the mean torso height in the crowd), and $z = 163 \text{ cm}$ (the torso height of the tallest pedestrian), respectively. The total areas covered by pedestrian bodies in 2D are indicated.

369
370
371

```
./run_mechanical_tests
```

372

The script will prompt you to enter the path to your [FFmpeg](#) application, which is required to generate movies from the simulation files.

373

374

The results of the eight tests will appear in the `tests/mechanical_layer/movies` directory.

375

You will then have the opportunity to review all the videos and determine if they meet your expectations. The eight test scenarios are as follows:

376

377

- ★ **Agent pushing another agent** (`test_push_agent_agent` folder)

378

Tests the force orthogonal to the contact surface, representing a damped spring interaction between two agents.

379

380

- ★ **Agent colliding with a wall** (`test_push_agent_wall` folder)

381

Tests the force orthogonal to the contact surface, representing a damped spring interaction between an agent and a wall.

382

383

- ★ **Agent sliding over other agents** (`test_slip_agent_agent` folder)

384

Tests the Coulomb friction interaction between two agents as one slides over the other.

385

- ★ **Agent sliding over a wall** (`test_slip_agent_wall` folder)

386

Tests the Coulomb friction interaction between an agent and a wall as the agent slides along it.

387

- 388 ★ **Agent translating and relaxing** (test_t_translation folder)
 389 Tests the behaviour as an agent undergoes a translation and gradually relaxes to a sta-
 390 tionary state (no motion), due to the fluid-like force with the damping coefficient of
 391 $1/t^{(\text{translation})}$.
- 392 ★ **Agent rotating and relaxing** (test_t_rotation folder)
 393 Tests the behaviour as an agent rotates and gradually relaxes to a stationary state (no
 394 motion), due to the fluid-like torque with the damping coefficient of $1/t^{(\text{rotation})}$.
- 395 ★ **Agent rolling over other agents without sliding** (test_tangential_spring_agent_agent
 396 folder)
 397 Tests the force tangential to the contact surface, representing a damped spring interac-
 398 tion between two agents.
- 399 ★ **Agent rolling over a wall without sliding** (test_tangential_spring_agent_wall
 400 folder)
 401 Tests the force tangential to the contact surface, representing a damped spring interac-
 402 tion between an agent and a wall.
- 403 These tests yielded the expected outcomes (the videos are provided in the supplemental ma-
 404 terial [30]).

405 4.3 Practical case study

406 We will detail here how to perform a simulation of a crowd evacuation that achieves *mechan-*
 407 *ical* realism, albeit (deliberately) naïve as for the decisional component. This foundational
 408 example serves as a basis for the future integration of a more advanced decision-making layer
 409 (not addressed in this article), which would enable the quantitative replication of empirical
 410 observables—such as exit times—recorded in evacuation scenarios. The parameters employed
 411 in this simulation are detailed in Tab. 1, and illustrative snapshots can be found in Fig. 9.

Parameter	Description	Value
$t^{(\text{transl})}$	Relaxation time for translational motion	0.5 s
$t^{(\text{rot})}$	Relaxation time for rotational motion	0.5 s
E_{body}	Young modulus for the wall (human naked material)	$2.6 \times 10^6 \text{ kg/s}^2$
G_{body}	Shear modulus for the wall (human naked material)	$7.5 \times 10^5 \text{ kg/s}^2$
$\gamma_{\text{body}}^{\perp}$	Damping for orthogonal contact in pedestrian-pedestrian contact in the di- rection orthogonal to the surface contact	$1.3 \times 10^4 \text{ kg/s}$
$\gamma_{\text{body}}^{\parallel}$	Damping for tangential contact in pedestrian-pedestrian contact in the di- rection parallel to the surface contact	$1.3 \times 10^4 \text{ kg/s}$
$\mu_{\text{body}}^{\text{dyn}}$	Kinetic friction for pedestrian-pedestrian contact	0.5
E_{wall}	Young modulus for the wall (concrete)	$1.7 \times 10^{10} \text{ kg/s}^2$
G_{wall}	Shear modulus for the wall (concrete)	$7.1 \times 10^9 \text{ kg/s}^2$
$\gamma_{\text{wall}}^{\perp}$	Damping for orthogonal contact in pedestrian-wall contact in the direction orthogonal to the surface contact	$1.3 \times 10^4 \text{ kg/s}$
$\gamma_{\text{wall}}^{\parallel}$	Damping for tangential contact in pedestrian-wall contact in the direction parallel to the surface contact	$1.3 \times 10^4 \text{ kg/s}$
$\mu_{\text{wall}}^{\text{dyn}}$	Kinetic friction for pedestrian-wall contact	0.5

Table 1: Parameter values used in the practical case study. The units of the elastic moduli are for 2D systems.

412 413 Set the working environment and generate the desired configuration files

414
 415 Start by creating your desired crowd using the online platform, for example, eight pedestrians
 416 with anthropometric characteristics from the [ANSURII](#) database, arranged in a tightly packed
 417 configuration. Download the resulting configuration files to your local system. For instance,

you can create a new directory called `Trial_1` and navigate into it. Create and configure a `Parameters.xml` file in this directory. Within `Trial_1`, add two subdirectories named `static` and `dynamic`. Place the configuration files obtained from the online platform into their respective folders. For reference, an example of the recommended directory structure is shown below:

```
.
|-- Parameters.xml
|-- static/
|   |-- Agents.xml
|   |-- Geometry.xml
|   |-- Materials.xml
|-- dynamic/
|   |-- AgentDynamics.xml
```

Finally, modify the `Geometry.xml` file to define the desired geometry, and adjust the `AgentDynamics.xml` file to set the appropriate initial propulsion force and torque. Refer to App. C for the configuration files used in this practical case.

Run the simulation

Above all, you need to navigate to the root of the `src/mechanical_layer` directory and build the project:

```
cmake -H. -Bbuild -DBUILD_SHARED_LIBS=ON
cmake --build build
```

Run the Python code provided below, making any necessary modifications to suit your needs. The simulation results will be saved automatically in the `outputXML/` directory. Each output file follows the naming pattern `AgentDynamics output t=TIME_VALUE.xml`, where `TIME_VALUE` indicates the corresponding simulation time or a unique identifier for that run.

```
import ctypes
from pathlib import Path
import numpy as np
from shutil import copyfile
import xml.etree.ElementTree as ET

# === Simulation Parameters ===
dt = 0.1 # Time step for the decisional layer (matches "TimeStep" in Parameters.xml)
Ndt = 100 # How many dt will be performed in total

# === Paths Setup ===
outputPath = Path("outputXML/") # Directory to store output XML files
inputPath = Path("inputXML/") # Directory to store input XML files
outputPath.mkdir(parents=True, exist_ok=True) # Create directories if they don't exist
inputPath.mkdir(parents=True, exist_ok=True)

# === Loading the External Mechanics Library ===
# Adjust filename for OS (.so for Linux, .dylib for macOS)
Clibrary = ctypes.CDLL("../src/mechanical_layer/build/libCrowdMechanics.dylib")
agentDynamicsFilename = "AgentDynamics.xml"

# Prepare the list of XML files that will be passed to the DLL/shared library
files = [
    b"Parameters.xml",
    b"Materials.xml",
    b"Geometry.xml",
    b"Agents.xml",
    agentDynamicsFilename.encode("ascii"), # Convert filename to bytes (required by ctypes)
]
nFiles = len(files) # Number of configuration files to be passed
filesInput = (ctypes.c_char_p * nFiles)() # Create a ctypes array of string pointers
filesInput[:] = files # Populate array with the XML file names

# === Main Simulation Loop ===
for t in range(Ndt):
    print("Looping the Crowd mechanics engine - t=%.1fs..." % (t * dt))

    # 1. Save the current AgentDynamics file as input for this step (can be used for analysis later)
    copyfile("dynamic/" + agentDynamicsFilename, str(inputPath) + rf"/AgentDynamics input t={t * dt:.1f}.xml")

    # 2. Call the external mechanics engine, passing in the list of required XML files
```

```

492     Clibrary.CrowdMechanics(filesInput)
493
494     # 3. Save the updated AgentDynamics output to results folder (can be used for analysis later)
495     copyfile("dynamic/" + agentDynamicsFilename, str(outputPath) + rf"/AgentDynamics output t={(t + 1) * dt:.1f}.xml")
496
497     # 4. If the simulation produced an AgentInteractions.xml file, save that as well (optional output)
498     try:
499         copyfile("dynamic/AgentInteractions.xml", str(outputPath) + rf"/AgentInteractions t={(t + 1) * dt:.1f}.xml")
500     except FileNotFoundError:
501         # If the AgentInteractions file does not exist, skip copying
502         pass
503
504     # === Decision/Controller Layer for Next Step ===
505     # Read the output AgentDynamics XML as input for the next run.
506     # This is where you (or another program) can set new forces/moments for each agent for the next simulation step.
507     XMLtree = ET.parse("dynamic/" + agentDynamicsFilename)
508     agentsTree = XMLtree.getroot()
509
510     # -- Assign random forces/moments to each agent --
511     for agent in agentsTree:
512         # Create new <Dynamics> tag for the agent (as the output file doesn't have it)
513         dynamicsItem = ET.SubElement(agent, "Dynamics")
514
515         # Assign random force, and random moment
516         dynamicsItem.attrib["Fp"] = f"{np.random.normal(loc=200, scale=200):.2f},{np.random.normal(loc=0, scale=50):.2f}"
517         ↪ "
518         dynamicsItem.attrib["Mp"] = f"{np.random.normal(loc=0, scale=5):.2f}"
519
520     # Write the modified XML back, to be used in the next iteration
521     XMLtree.write("dynamic/" + agentDynamicsFilename)
522     # =====
523
524     # After all simulation steps are complete, print a final message.
525     print(f"Loop terminated at t={Ndt * dt:.1f}s!")
526

```

527

528 Generate plots and create a video from output files

529

530 A plot of the scene can be generated from each input/output file under PNG format using
531 the Python wrapper. To begin, you need to install the required Python packages, which you
532 can quickly do by setting up a virtual environment using [uv](#) as follows (from the root directory
533 of the project):

534

535

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537

538

```

python -m pip install --upgrade pip
pip install uv
uv sync

```

539 You can then run the following Python script within your working environment:

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```

import os
import matplotlib.pyplot as plt
import configuration.backup.dict_to_xml_and_reverse as fun_xml # For converting XML to dictionary and vice versa
from configuration.models.crowd import create_agents_from_dynamic_static_geometry_parameters # For creating agents
↪ based on XML data
from streamlit_app.plot import plot # For plotting crowd data

# === Simulation Parameters ===
dt = 0.1 # Time step for the decisional layer (matches "TimeStep" in Parameters.xml)
Ndt = 100 # How many dt will be performed in total

# === Prepare the folders ===
# Define the paths to the folders you'll use
outputPath = Path("outputXML/")
staticPath = Path("./static")
plotsPath = Path("./plots")
plotsPath.mkdir(parents=True, exist_ok=True) # Create plots directory if it doesn't exist

# Remove any old '.png' files in the plots directory
for file in plotsPath.glob("*.png"):
    os.remove(file)

# === Load static XML files ===
# Read the Agents.xml file as a string and convert it to a dictionary
with open(staticPath / "Agents.xml", encoding="utf-8") as f:
    crowd_xml = f.read()
static_dict = fun_xml.static_xml_to_dict(crowd_xml)

# Read the Geometry.xml file as a string and convert it to a dictionary
with open(staticPath / "Geometry.xml", encoding="utf-8") as f:
    geometry_xml = f.read()
geometry_dict = fun_xml.geometry_xml_to_dict(geometry_xml)

# === Loop over time steps ===
for t in range(Ndt):
    current_time = (t + 1) * dt

    # Check if the dynamics file exists; if not, skip to the next time step

```

```

579     dynamics_file = outputPath / f"AgentDynamics output t={current_time:.1f}.xml"
580     if not dynamics_file.exists():
581         print(f"Warning: {dynamics_file} not found, skipping.")
582         continue
583
584     # === Read and process the dynamics XML file ===
585     # Read the current dynamics XML file as a string and convert it to a dictionary
586     with open(dynamics_file, encoding="utf-8") as f:
587         dynamic_xml = f.read()
588         dynamic_dict = fun_xml.dynamic_xml_to_dict(dynamic_xml)
589
590     # Create a crowd object using the configuration files data
591     crowd = create_agents_from_dynamic_static_geometry_parameters(
592         static_dict=static_dict,
593         dynamic_dict=dynamic_dict,
594         geometry_dict=geometry_dict,
595     )
596
597     # Plot and save the crowd as a PNG file
598     plot.display_crowd2D(crowd)
599     plt.savefig(plotsPath / rf"crowd2D_t={t:d}.png", dpi=300, format="png")
600     plt.close()

```

602 All of the PNG images can then be combined into a video using [FFmpeg](#). Some example snap-
603 shots are shown in Fig. 9, and the full video is provided in the supplemental materials [30].

604 4.4 Extension to arbitrary shapes

605 This software was designed so that further developments can easily be implemented, partic-
606 ularly to include a wider variety of agents. To prove this point, we implemented bicycles in
607 the 2D agent generation on the online application [40]. To access this feature, navigate to
608 the CROWD tab, then in the sidebar under DATABASE ORIGIN, select the Custom statistics
609 option, and set the desired proportion of bicycles within the crowd. The bicycle agent has
610 been simplified to two overlapping rectangular polygons: one representing the front and rear
611 wheels, and the other representing the seated rider and handlebars. The statistics of the di-
612 mensions of these shapes are adjustable. Note, however, that the simulation code does not
613 model the mechanical interactions with bicycles, which we consider less relevant and more
614 complex than those between pedestrians. An example of such a heterogeneous crowd is shown
615 in Fig. 10.

616 The configuration file synthesising the crowd can be downloaded in XML format; it is sim-
617 pler than the configuration files for a pedestrian-only crowd. The file includes a list of agents,
618 each containing the following information: type (either pedestrian or bike), Id (an integer),
619 Moment of inertia (in $\text{kg}\cdot\text{m}^2$), FloorDamping ($t^{(\text{transl})}$), AngularDamping ($t^{(\text{rot})}$), and
620 Shapes. For agents of type bike, the Shapes tag contains two tags: bike (corresponding to
621 the front and rear wheels) and rider (corresponding to the human on the bicycle and the han-
622 dlebars). Within the bike tag, several other tags are included: type (rectangle), material
623 (iron, human clothes, etc.), min_x, min_y, max_x, and max_y, which transparently define
624 the rectangle's boundaries in absolute coordinates. The rider tag follows a similar structure.
625 For agents of type pedestrian, a similar structure is used. However, within the Shapes
626 tag, there are sub-tags disk0, disk1, up to disk4, each of which specifies the following
627 attributes: type (disk), radius, material, and x, y (the position of the disk's centre in
628 absolute coordinates).

629 5 Conclusion

630 In summary, we have released an open-source numerical tool to help modellers simulate the
631 dynamics of pedestrians in 2D and visualise the output in 2D and 3D. This tool is *not* a pedes-
632 trian simulation software (because the decisional components, notably the desired speeds and
633 directions, should be given as input), but it adds a substantial contribution to the field, espe-
634 cially for the study of dense crowds, in that it promotes realistic 2D projections of pedestrians,

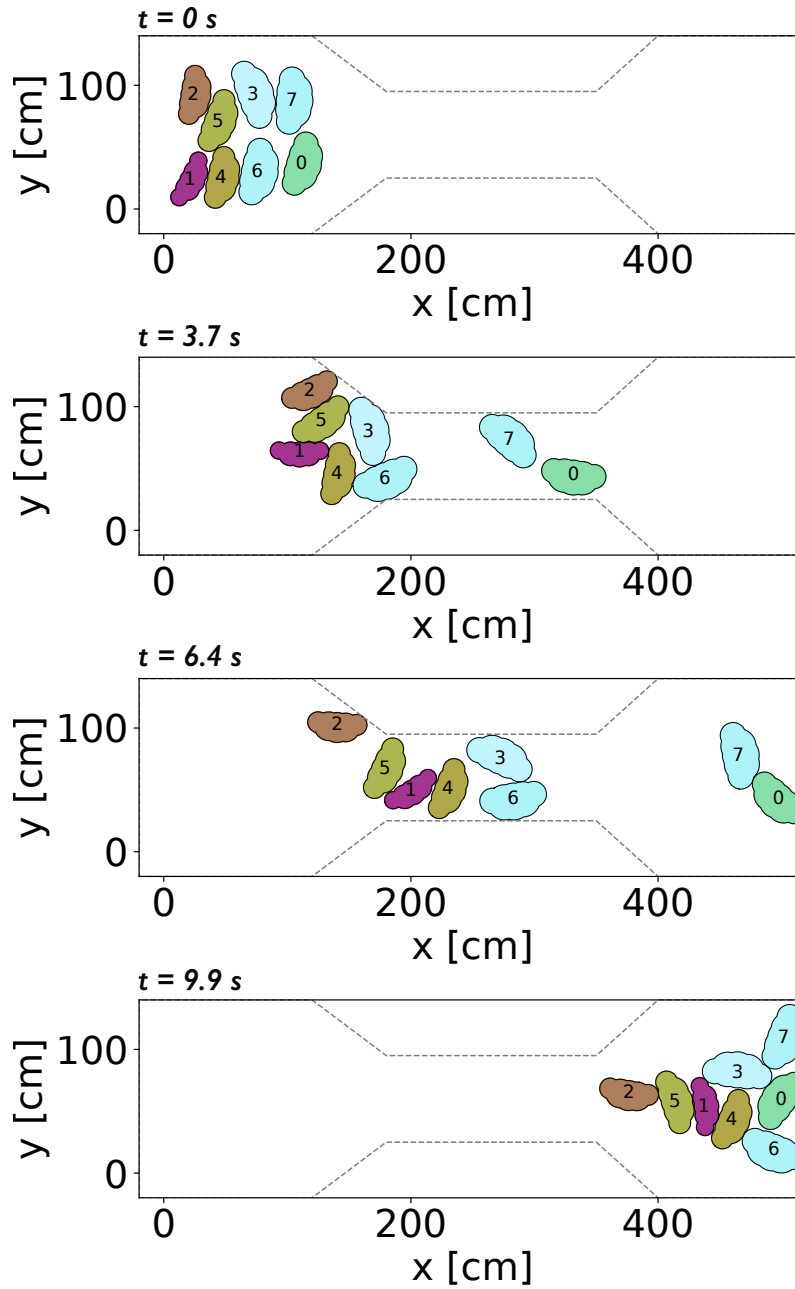


Figure 9: Four snapshots illustrating a crowd simulation in which eight pedestrians move from one room to another through a narrow corridor. The simulation uses a simple decisional model, where each pedestrian’s propulsion force \mathbf{F}_p and torque τ_p are randomly sampled from a normal distribution: $\mathbf{F}_{p,x} \sim \mathcal{N}(200, 150) \mid \mathbf{F}_{p,y} \sim \mathcal{N}(0, 20) \mid \tau_p \sim \mathcal{N}(0, 10)$. **Top panel:** shows the initial configuration at the start of the simulation. **Second panel ($t = 3.7\text{s}$):** highlights jamming at the corridor entrance; arch-like formations—referred to as ‘stress arcs’—have developed, impeding entry into the corridor. **Third panel ($t = 6.4\text{s}$):** the stress arcs have lifted, and pedestrians walk within the corridor almost freely. **Bottom panel:** depicts the final state at the end of the simulation.

635 grounded in anthropometric data and much more faithful than the typical circular assumption,
 636 and it computes contact forces derived from Physics. To make the code as broadly accessible
 637 to the public as possible, we have released an online platform for the generation and visual-

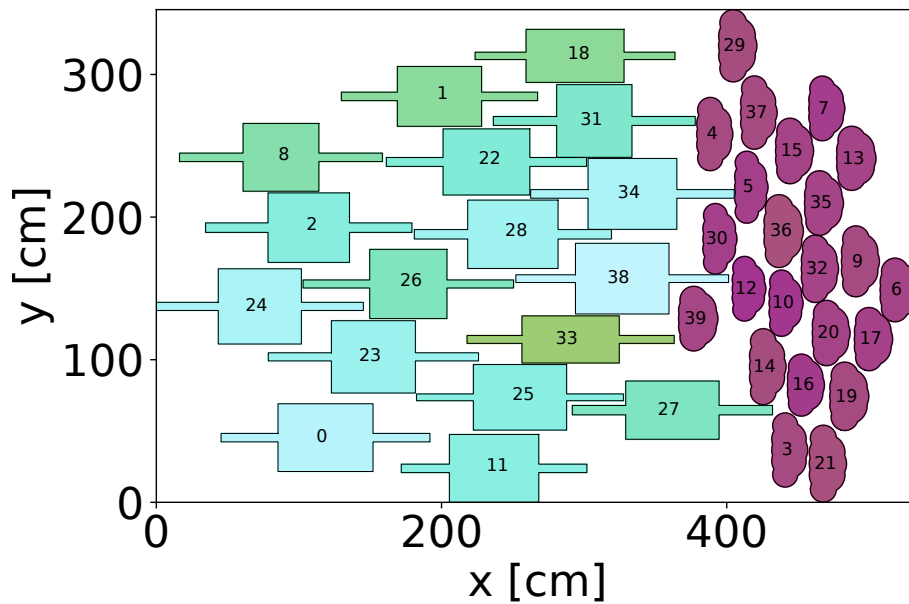


Figure 10: Heterogeneous crowd of 40 agents (17 bicycles + 23 pedestrians) with uniform orientation. The colour encodes agent area using the Hawaii colour map from cmcrameri [41]: transitioning from purple (smallest areas) to blue (largest areas). This example is not intended to be realistic, but rather to showcase that the pedestrian generation code can be easily generalised.

638 isation of agents, a computationally efficient C++ library for the dynamical simulations, and
639 an easy-to-use Python wrapper to run all scripts.

640 To let the tool evolve with the field, a generic XML format for configuration files has been
641 proposed. Currently, the tool can only generate bare or clothed adult men and women, as well
642 as cyclists. However, thanks to the generic file format, other shapes may be included in the
643 future, such as children, people carrying a backpack, and people pushing a pushchair. Further
644 in the future, it may also become relevant to extend the mechanical computations of contact
645 forces to 3D.

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660

661

662 A Equation of motion

663 A.1 Mechanical interactions

664 Consider two pedestrians, i and j , represented by sets of disks $s^{(i)}$ and $s^{(j)}$ respectively. Each
 665 disk center s^i of pedestrian i is positioned relative to pedestrian i 's center of mass G_i through
 666 the displacement vector $\Delta_{i \rightarrow s^{(i)}}$, which points toward $s^{(i)}$ (see Fig. 11a). The pedestrian's
 667 orientation is defined by the normal vector to the line connecting their first and last disks (see
 668 Fig. 11c). The CoM of pedestrian i moves with a translational velocity \mathbf{v}_i , and the pedestrian
 669 rotates with an angular velocity ω_i .

670 A.1.1 Forces acting on the pedestrian centre of mass

671 The motion of a pedestrian i can be broken down into two components: the motion of its
 672 **Center of Mass (CoM)** and rotational motion. The motion of the CoM is determined by applying
 673 the fundamental principle of dynamics at that point. When the shape $s^{(i)}$ of pedestrian i (with
 674 radius $R_{s^{(i)}}$ and position $\mathbf{r}_{s^{(i)}}$) comes into contact with the shape $s^{(j)}$ of pedestrian j (with radius
 675 $R_{s^{(j)}}$ and position $\mathbf{r}_{s^{(j)}}$), as illustrated in Fig. 11a, pedestrian i experiences the following forces
 676 (analogous forces are applied in the case of contact with a wall, illustrated in Fig. 11b):

677 ★ A damped-spring force orthogonal to the surface contact denoted as $\mathbf{F}_{s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}}$, split into
 678 its spring part denoted as $\mathbf{F}_{\text{spring}, s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}}$, linear with the interpenetration depth and a
 679 damping part denoted as $\mathbf{F}_{\text{damping}, s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}}$, that can be expressed as:

$$\begin{aligned}
 680 \quad \triangleright \mathbf{F}_{\text{spring}, s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}} &= \begin{cases} k_{\text{body}}^{\perp} h_{s^{(i) s^{(j)}}} \mathbf{n}_{s^{(j) \rightarrow s^{(i)}}} & \text{if } h_{s^{(i) s^{(j)}}} = R_{s^{(i)}} + R_{s^{(j)}} - |\mathbf{r}_{s^{(j)} \rightarrow s^{(i)}}| > 0 \text{ (i.e. an overlap occurs)} \\ \mathbf{0} & \text{otherwise} \end{cases} \\
 681 \quad \triangleright \mathbf{F}_{\text{damping}, s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}} &= \begin{cases} -\gamma_{\text{body}}^{\perp} \mathbf{v}_{ij}^{\perp} & \text{if } h_{s^{(i) s^{(j)}}} > 0 \text{ (i.e. an overlap occurs)} \\ \mathbf{0} & \text{otherwise} \end{cases}
 \end{aligned}$$

682 where $\mathbf{n}_{s^{(j) \rightarrow s^{(i)}}}$ denotes the unitary vector normal to the surface contact pointing towards
 683 $s^{(i)}$, \mathbf{v}_{ij}^{\perp} describes the relative velocity at the contact point C along the direction normal
 684 to the surface contact and $\mathbf{r}_{s^{(j)} \rightarrow s^{(i)}}$ is the relative position of the two shapes in contact
 685 pointing towards shape $s^{(i)}$. k_{body}^{\perp} represents the spring constant and $\gamma_{\text{body}}^{\perp}$ the damping
 686 intensity in the normal direction for body-body contacts.

687 ★ A force, tangential to the contact surface that acts in the direction opposite to the slip.
 688 A straightforward way to model this force is through Coulomb interaction to describe
 689 the stick and slip mechanism, and a damped spring to more precisely describe the stick
 690 phase. It can be written as:

$$\mathbf{F}_{s^{(j) \rightarrow s^{(i)}}}^{\parallel \text{contact}} = \begin{cases} k_{\text{body}}^{\parallel} \delta s \frac{-\mathbf{v}_{ij}^{\parallel}}{|\mathbf{v}_{ij}^{\parallel}|} - \gamma_{\text{body}}^{\parallel} \mathbf{v}_{ij}^{\parallel} & \text{if } k_{\text{body}}^{\parallel} \delta s + \gamma_{\text{body}}^{\parallel} |\mathbf{v}_{ij}^{\parallel}| < \mu_{\text{body}}^{\text{dyn}} |\mathbf{F}_{s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}}| \text{ (stick)} \\ \mu_{\text{body}}^{\text{dyn}} |\mathbf{F}_{s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}}| \frac{-\mathbf{v}_{ij}^{\parallel}}{|\mathbf{v}_{ij}^{\parallel}|} & \text{otherwise (slip)} \end{cases} \quad (\text{A.1})$$

691 where δs represents the spring elongation and can be written as $\delta s = \left| \int_0^{\text{contact duration}} \mathbf{v}_{ij}^{\parallel} dt \right|$

692 and $\mu_{\text{body}}^{\text{dyn}}$ denotes the dynamic friction coefficient. The force can be reshaped in a more

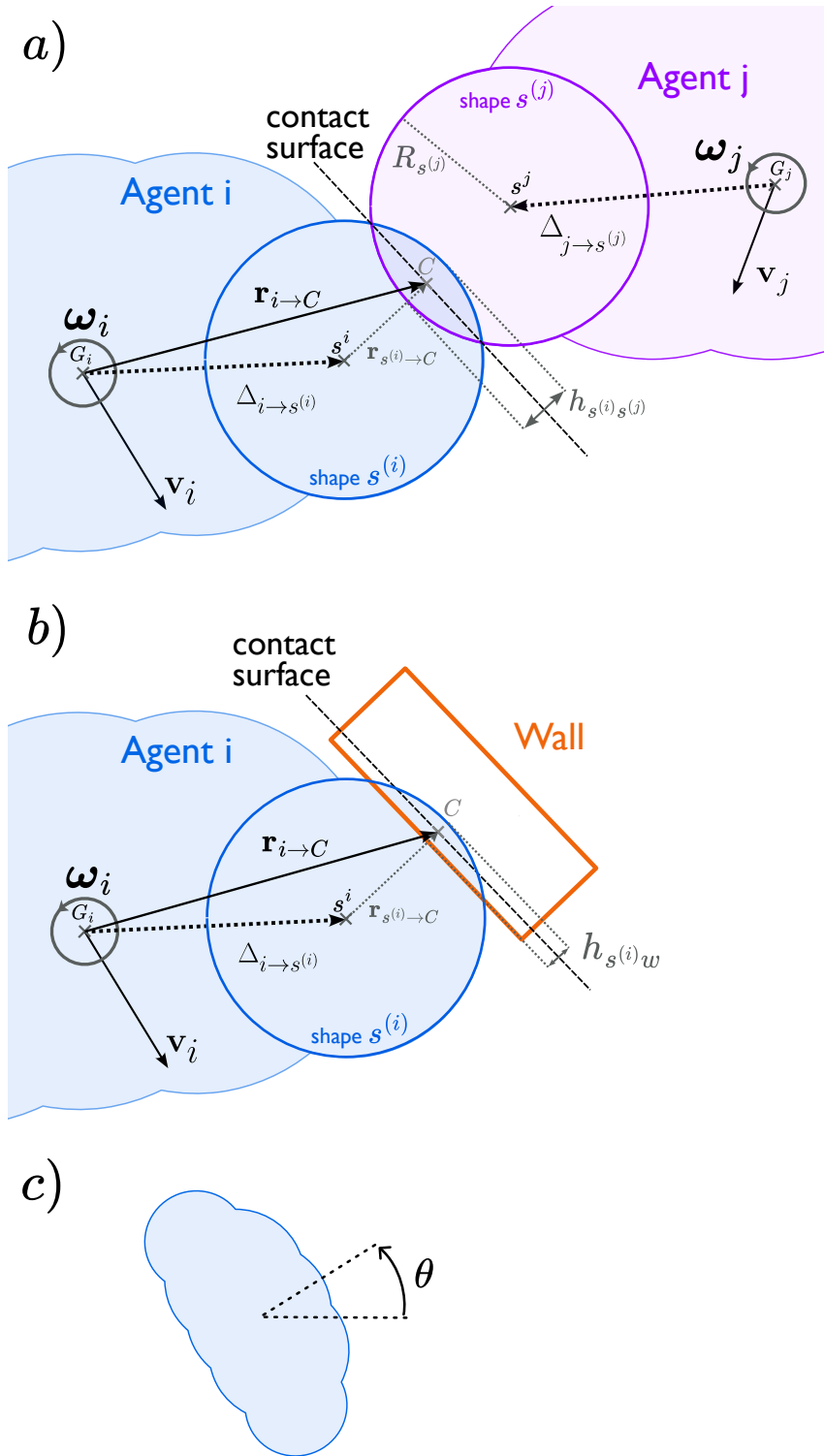


Figure 11: **(a)** Contact between two pedestrian bodies; **(b)** Contact between a pedestrian body and a wall; **(c)** Definition of pedestrian orientation. The contact surface is represented by the bisector of the shortest line segment connecting either the contours of two composite disks or the contour of a composite disk and a wall. The contact point C is located at the midpoint of this segment.

$$\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\parallel \text{contact}} = \min \left(k_{\text{body}}^{\parallel} \delta s + \gamma_{\text{body}}^{\parallel} |\mathbf{v}_{ij}^{\parallel}|, \mu_{\text{body}}^{\text{dyn}} |\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}}| \right) \frac{-\mathbf{v}_{ij}^{\parallel}}{|\mathbf{v}_{ij}^{\parallel}|} \quad (\text{A.2})$$

- 694 ★ A self-propelling force \mathbf{F}_p , that converts decisions into actions;
- 695 ★ A fluid friction force, encompassing the effective backward friction with the ground over
- 696 a simulation step cycle, controlled by the deformation of the body (biomechanical dis-
- 697 sipation) expressed as $-m_i \mathbf{v}_i / \tau^{(\text{transl})}$, where $\tau^{(\text{transl})}$ is the characteristic relaxation time
- 698 to the rest state.

699 A.1.2 Torque for rotation of a pedestrian

700 The rotational motion of a pedestrian is obtained by applying the angular momentum theorem
 701 to the pedestrian's **Center of Mass (CoM)**. This is done in its principal inertia base, projected
 702 along the z-axis (the out-of-plane axis). The pedestrian experiences torque due to the forces
 703 that are normal and tangential to the contact surface:

$$\tau_{G_i, s^{(j)} \rightarrow s^{(i)}} = \left\{ \mathbf{r}_{i \rightarrow C} \times \left(\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\parallel \text{contact}} + \mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} \right) \right\} \cdot \mathbf{u}_z \quad (\text{A.3})$$

704 The self-propelling force and the fluid friction force act directly on the **CoM**, resulting in zero
 705 torque. To account for decision-making, a decisional torque τ_p is applied. Finally, analogous
 706 to the **CoM** equation, a fluid friction force accounting for floor contact and all mechanical
 707 dissipation mechanisms (including biomechanical effects) is incorporated as $-I_i \omega_i / \tau^{(\text{rot})}$. The
 708 computation of the moment of inertia I_i is detailed in App. A.2.

709 A.2 Moment of inertia calculation

710 Each pedestrian in our synthetic crowd is represented as a combination of five disks. While an
 711 analytical formula for the moment of inertia of such a configuration can be derived, it is quite
 712 cumbersome to write and implement numerically. Instead, we approximate the pedestrian's
 713 boundary using an N -sided polygon, defined by the set of vertices:

$$\{(x_1, y_1), (x_2, y_2), \dots, (x_{N+1}, y_{N+1}) : (x_1, y_1) = (x_{N+1}, y_{N+1})\}, \quad (\text{A.4})$$

714 where $(x_1, y_1) = (x_{N+1}, y_{N+1})$ ensures the polygon is closed. Assuming pedestrian i 's mass m_i
 715 is uniformly distributed within the polygon (yielding homogeneous mass density $\rho_i = m_i / \text{Polygon Area}$),
 716 the moment of inertia I_i can be calculated via [42]:

$$I_i = \frac{\rho_i}{12} \sum_{j=1}^N (x_j y_{j+1} - x_{j+1} y_j) (x_j^2 + x_j x_{j+1} + x_{j+1}^2 + y_j^2 + y_j y_{j+1} + y_{j+1}^2). \quad (\text{A.5})$$

717 A.3 Mechanical equations summary

718 Pedestrian **CoM** dynamics

$$\begin{aligned} m_i \frac{d\mathbf{v}_i}{dt} = & \mathbf{F}_p - m_i \frac{\mathbf{v}_i}{\tau^{(\text{transl})}} + \sum_{(s^{(j)}, s^{(i)}) \in \mathcal{C}_i^{(\text{ped})}} \left(\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\parallel \text{contact}} + \mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} \right) \\ & + \sum_{(w, s^{(i)}) \in \mathcal{C}_i^{(\text{wall})}} \left(\mathbf{F}_{w \rightarrow s^{(i)}}^{\parallel \text{contact}} + \mathbf{F}_{w \rightarrow s^{(i)}}^{\perp \text{contact}} \right) \end{aligned} \quad (\text{A.6})$$

719 Interaction forces with a pedestrian

$$\begin{aligned}
\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\parallel \text{contact}} &= \min \left(k_{\text{body}}^{\parallel} \delta s + \gamma_{\text{body}}^{\parallel} \left| \mathbf{v}_{ij}^{\parallel} \right|, \mu_{\text{body}}^{\text{dyn}} \left| \mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} \right| \right) \frac{-\mathbf{v}_{ij}^{\parallel}}{\left| \mathbf{v}_{ij}^{\parallel} \right|} \\
\mathbf{F}_{s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} &= \mathbf{F}_{\text{spring}, s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} + \mathbf{F}_{\text{damping}, s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} \\
\mathbf{F}_{\text{spring}, s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} &= \begin{cases} k_{\text{body}}^{\perp} h_{s^{(i)}s^{(j)}} \mathbf{n}_{s^{(j)} \rightarrow s^{(i)}} & \text{if } h_{s^{(i)}s^{(j)}} > 0 \text{ (i.e. an overlap occurs)} \\ \mathbf{0} & \text{otherwise} \end{cases} \\
\mathbf{F}_{\text{damping}, s^{(j)} \rightarrow s^{(i)}}^{\perp \text{contact}} &= \begin{cases} -\gamma_{\text{body}}^{\perp} \mathbf{v}_{ij}^{\perp} & \text{if } h_{s^{(i)}s^{(j)}} > 0 \text{ (i.e. an overlap occurs)} \\ \mathbf{0} & \text{otherwise} \end{cases}
\end{aligned} \tag{A.7}$$

720 where

$$\begin{aligned}
h_{s^{(i)}s^{(j)}} &= R_{s^{(i)}} + R_{s^{(j)}} - \left| \mathbf{r}_{s^{(i)} \rightarrow s^{(j)}} \right| \\
\delta s &= \left| \int_0^{\text{contact duration}} \mathbf{v}_{ij}^{\parallel} dt \right| \\
\mathbf{v}_{ij}^{\parallel} &= \mathbf{v}_{ij} - \mathbf{v}_{ij}^{\perp} \\
\mathbf{v}_{ij}^{\perp} &= (\mathbf{v}_{ij} \cdot \mathbf{n}_{s^{(i)} \rightarrow s^{(j)}}) \mathbf{n}_{s^{(i)} \rightarrow s^{(j)}} \\
\mathbf{v}_{ij} &= \mathbf{v}_{i,C} - \mathbf{v}_{j,C} \\
\mathbf{v}_{i,C} &= \mathbf{v}_i + \boldsymbol{\omega}_i \times \mathbf{r}_{i \rightarrow C} \\
\mathbf{r}_{i \rightarrow C} &= \boldsymbol{\Delta}_{i \rightarrow s^{(i)}} + \mathbf{r}_{s^{(i)} \rightarrow C} \\
\mathbf{n}_{s^{(i)} \rightarrow s^{(j)}} &= \frac{\mathbf{r}_{s^{(i)} \rightarrow s^{(j)}}}{\left| \mathbf{r}_{s^{(i)} \rightarrow s^{(j)}} \right|} \\
\mathbf{r}_{s^{(i)} \rightarrow s^{(j)}} &= \mathbf{r}_j + \boldsymbol{\Delta}_{j \rightarrow s^{(j)}} - (\mathbf{r}_i + \boldsymbol{\Delta}_{i \rightarrow s^{(i)}}) \\
\mathbf{r}_{s^{(i)} \rightarrow C} &= \left(R_{s^{(i)}} - \frac{h_{s^{(i)}s^{(j)}}}{2} \right) \mathbf{n}_{s^{(i)} \rightarrow s^{(j)}}
\end{aligned} \tag{A.8}$$

721 Interaction forces with wall

$$\begin{aligned}
\mathbf{F}_{w \rightarrow s^{(i)}}^{\parallel \text{contact}} &= \min \left(k_{\text{wall}}^{\parallel} \delta s_w + \gamma_{\text{wall}}^{\parallel} \left| \mathbf{v}_{s^{(i)}w}^{\parallel} \right|, \mu_{\text{wall}}^{\text{dyn}} \left| \mathbf{F}_{w \rightarrow s^{(i)}}^{\perp \text{contact}} \right| \right) \frac{-\mathbf{v}_{iw}^{\parallel}}{\left| \mathbf{v}_{iw}^{\parallel} \right|} \\
\mathbf{F}_{w \rightarrow s^{(i)}}^{\perp \text{contact}} &= \mathbf{F}_{\text{spring}, w \rightarrow s^{(i)}}^{\perp \text{contact}} + \mathbf{F}_{\text{damping}, w \rightarrow s^{(i)}}^{\perp \text{contact}} \\
\mathbf{F}_{\text{spring}, w \rightarrow s^{(i)}}^{\perp \text{contact}} &= \begin{cases} k_{\text{wall}}^{\perp} h_{s^{(i)}w} \mathbf{n}_{w \rightarrow s^{(i)}} & \text{if } h_{s^{(i)}w} > 0 \text{ (i.e. an overlap occurs)} \\ \mathbf{0} & \text{otherwise} \end{cases} \\
\mathbf{F}_{\text{damping}, w \rightarrow s^{(i)}}^{\perp \text{contact}} &= \begin{cases} -\gamma_{\text{wall}}^{\perp} \mathbf{v}_{iw}^{\perp} & \text{if } h_{s^{(i)}w} > 0 \text{ (i.e. an overlap occurs)} \\ \mathbf{0} & \text{otherwise} \end{cases}
\end{aligned} \tag{A.9}$$

722 where

$$\begin{aligned}
h_{s(i)w} &= R_{s(i)} - |\mathbf{r}_{s(i) \rightarrow w}| \\
\delta s_w &= \left| \int_0^{\text{contact duration}} \mathbf{v}_{iw}^{\parallel} dt \right| \\
\mathbf{v}_{iw}^{\parallel} &= \mathbf{v}_{i,C} - \mathbf{v}_{iw}^{\perp} \\
\mathbf{v}_{iw}^{\perp} &= (\mathbf{v}_{i,C} \cdot \mathbf{n}_{s(i) \rightarrow w}) \mathbf{n}_{s(i) \rightarrow w} \\
\mathbf{v}_{i,C} &= \mathbf{v}_i + \boldsymbol{\omega}_i \times \mathbf{r}_{i \rightarrow C} \\
\mathbf{n}_{s(i) \rightarrow w} &= \frac{\mathbf{r}_{s(i) \rightarrow w}}{|\mathbf{r}_{s(i) \rightarrow w}|} \\
\mathbf{r}_{i \rightarrow C} &= \Delta_{i \rightarrow s(i)} + \mathbf{r}_{s(i) \rightarrow C} \\
\mathbf{r}_{s(i) \rightarrow C} &= \left(R_{s(i)} - \frac{h_{s(i)w}}{2} \right) \mathbf{n}_{s(i) \rightarrow w} \\
\mathbf{r}_{s(i) \rightarrow w} &= \text{the vector from the center of } s^{(i)} \text{ to its nearest point on the wall } w
\end{aligned} \tag{A.10}$$

723 **Rotational dynamics**

$$\begin{aligned}
I_i \frac{d\boldsymbol{\omega}_i}{dt} &= \boldsymbol{\tau}_p - I_i \frac{\boldsymbol{\omega}_i}{t(\text{rot})} + \sum_{(s^{(j)}, s^{(i)}) \in \mathcal{C}_i^{(\text{ped})}} \boldsymbol{\tau}_{G_i, s^{(j) \rightarrow s^{(i)}}} \\
&+ \sum_{(s^{(j)}, s^{(i)}) \in \mathcal{C}_i^{(\text{wall})}} \boldsymbol{\tau}_{G_i, w \rightarrow s^{(i)}}
\end{aligned} \tag{A.11}$$

724 **Torques**

$$\begin{aligned}
\boldsymbol{\tau}_{G_i, s^{(j) \rightarrow s^{(i)}}} &= \left\{ \mathbf{r}_{i \rightarrow C} \times \left(\mathbf{F}_{s^{(j) \rightarrow s^{(i)}}}^{\parallel \text{contact}} + \mathbf{F}_{s^{(j) \rightarrow s^{(i)}}}^{\perp \text{contact}} \right) \right\} \cdot \mathbf{u}_z \\
\boldsymbol{\tau}_{G_i, w \rightarrow s^{(i)}} &= \left\{ \mathbf{r}_{i \rightarrow C} \times \left(\mathbf{F}_{w \rightarrow s^{(i)}}^{\parallel \text{contact}} + \mathbf{F}_{w \rightarrow s^{(i)}}^{\perp \text{contact}} \right) \right\} \cdot \mathbf{u}_z
\end{aligned} \tag{A.12}$$

725 B Mechanical layer: agent shortlisting

726 In order to save computing power, the mechanical layer begins by identifying a subset of the
727 agents, dubbed the “mechanically active agents”, for which a collision is likely/possible. The
728 remaining agents are thereby considered as having no chance to collide with anything else
729 during the execution of the code, and will therefore see their position evolve according to the
730 “relaxation” part of equation (1) only. The shortlisting is performed in two steps:

- 731 (i) For each agent i , we establish a list of *neighbouring* agents and walls based on
- 732 • the radius R_i of the agent – that is, the radius of the circle \mathcal{C}_i centred on the agent’s
 - 733 centre of mass, of which the agent’s global shape is circumscribed;
 - 734 • a global constant: the maximum – running – speed $v_{\max} = 7 \text{ m/s}$ of a pedestrian.

735 *Agent neighbours* of i will be defined as agents j for which the smallest distance between
736 the borders of the circles \mathcal{C}_i and \mathcal{C}_j is smaller than the distance traveled by both agents
737 at speed v_{\max} in a time TimeStep (ie twice the distance traveled at speed v_{\max} in a time
738 TimeStep).

739 *Wall neighbours* of i will be defined as walls for which the smallest distance between the
740 border of the circle \mathcal{C}_i and the wall is smaller than the distance travelled at speed v_{\max}
741 in a time TimeStep).

- 742 (ii) We look at new positions of all agents after a uniform motion over time TimeStep, with
743 velocity and angular velocity equal to

$$\mathbf{v}^{(0)} \mathbf{e}^{(\text{target})} = \frac{\mathbf{F}_p}{m_i} \mathbf{t}^{(\text{transl})} \quad \text{and} \quad \omega^{(0)} = \frac{\tau_p}{I_i} \mathbf{t}^{(\text{rot})},$$

and check for overlaps with neighbours. In case of overlap with a *wall neighbour*, the agent is considered “mechanically active”, and in case of an overlap with an *agent neighbour*, both agents are considered “mechanically active”. Furthermore, at the end of this process, we also add the *agent neighbours* of “mechanically active” agents.

Finally, agents with a significant difference between the three velocity components above and the ones of their current state – i.e. above 1 cm/s, are added to the list.

C Configuration files example

Parameters.xml file

```
751 <?xml version="1.0" encoding="utf-8"?>
752 <Parameters>
753   <Directories Static="./static/" Dynamic="./dynamic/" />
754   <Times TimeStep="0.1" TimeStepMechanical="5e-6" />
755 </Parameters>
```

Geometry.xml file

```
758 <?xml version="1.0" encoding="utf-8"?>
759 <Geometry>
760   <Dimensions Lx="5.40" Ly="1.60" />
761   <Wall Id="0" MaterialId="concrete">
762     <Corner Coordinates="-0.20,-0.20" />
763     <Corner Coordinates="1.20,-0.20" />
764     <Corner Coordinates="1.80,0.25" />
765     <Corner Coordinates="3.50,0.25" />
766     <Corner Coordinates="4.0,-0.2" />
767     <Corner Coordinates="5.20,-0.2" />
768     <Corner Coordinates="5.20,1.4" />
769     <Corner Coordinates="4.0,1.4" />
770     <Corner Coordinates="3.50,0.95" />
771     <Corner Coordinates="1.80,0.95" />
772     <Corner Coordinates="1.20,1.40" />
773     <Corner Coordinates="-0.20,1.40" />
774     <Corner Coordinates="-0.20,-0.20" />
775   </Wall>
776 </Geometry>
```

Materials.xml file

```
779 <?xml version="1.0" encoding="utf-8"?>
780 <Materials>
781   <Intrinsic>
782     <Material Id="concrete" YoungModulus="1.70e+10" ShearModulus="7.10e+09" />
783     <Material Id="human_clothes" YoungModulus="3.05e+06" ShearModulus="1.02e+06" />
784     <Material Id="human_naked" YoungModulus="2.60e+06" ShearModulus="7.50e+05" />
785   </Intrinsic>
786   <Binary>
787     <Contact Id1="concrete" Id2="concrete" GammaNormal="1.30e+04" GammaTangential="1.30e+04" KineticFriction="0.50" />
788     <Contact Id1="concrete" Id2="human_clothes" GammaNormal="1.30e+04" GammaTangential="1.30e+04" KineticFriction="0.50" />
789     <Contact Id1="concrete" Id2="human_naked" GammaNormal="1.30e+04" GammaTangential="1.30e+04" KineticFriction="0.50" />
790     <Contact Id1="human_clothes" Id2="human_clothes" GammaNormal="1.30e+04" GammaTangential="1.30e+04" KineticFriction="0.50" />
791     <Contact Id1="human_clothes" Id2="human_naked" GammaNormal="1.30e+04" GammaTangential="1.30e+04" KineticFriction="0.50" />
792     <Contact Id1="human_naked" Id2="human_naked" GammaNormal="1.30e+04" GammaTangential="1.30e+04" KineticFriction="0.50" />
793   </Binary>
794 </Materials>
```

Agents.xml file

```
803 <?xml version="1.0" encoding="utf-8"?>
804 <Agents>
805   <Agent Type="pedestrian" Id="0" Mass="90.72" Height="1.83" MomentOfInertia="2.05" FloorDamping="2.00" AngularDamping="2.00" />
806   <Shape Type="disk" Radius="0.098" MaterialId="human_naked" Position="-0.017,0.164" />
807 </Agents>
```



```

809     <Shape Type="disk" Radius="0.134" MaterialId="human_naked" Position="0.010,0.072"/>
810     <Shape Type="disk" Radius="0.141" MaterialId="human_naked" Position="0.015,0.000"/>
811     <Shape Type="disk" Radius="0.134" MaterialId="human_naked" Position="0.010,-0.072"/>
812     <Shape Type="disk" Radius="0.098" MaterialId="human_naked" Position="-0.017,-0.164"/>
813   </Agent>
814   <Agent Type="pedestrian" Id="1" Mass="68.04" Height="1.75" MomentOfInertia="1.18" FloorDamping="2.00" AngularDamping
815     ↳="2.00">
816     <Shape Type="disk" Radius="0.069" MaterialId="human_naked" Position="-0.017,0.167"/>
817     <Shape Type="disk" Radius="0.095" MaterialId="human_naked" Position="0.010,0.073"/>
818     <Shape Type="disk" Radius="0.100" MaterialId="human_naked" Position="0.015,0.000"/>
819     <Shape Type="disk" Radius="0.095" MaterialId="human_naked" Position="0.010,-0.073"/>
820     <Shape Type="disk" Radius="0.069" MaterialId="human_naked" Position="-0.017,-0.167"/>
821   </Agent>
822   <Agent Type="pedestrian" Id="2" Mass="74.39" Height="1.80" MomentOfInertia="1.39" FloorDamping="2.00" AngularDamping
823     ↳="2.00">
824     <Shape Type="disk" Radius="0.084" MaterialId="human_naked" Position="-0.017,0.156"/>
825     <Shape Type="disk" Radius="0.116" MaterialId="human_naked" Position="0.010,0.069"/>
826     <Shape Type="disk" Radius="0.121" MaterialId="human_naked" Position="0.015,0.000"/>
827     <Shape Type="disk" Radius="0.116" MaterialId="human_naked" Position="0.010,-0.069"/>
828     <Shape Type="disk" Radius="0.084" MaterialId="human_naked" Position="-0.017,-0.156"/>
829   </Agent>
830   <Agent Type="pedestrian" Id="3" Mass="115.67" Height="1.83" MomentOfInertia="2.97" FloorDamping="2.00"
831     ↳ AngularDamping="2.00">
832     <Shape Type="disk" Radius="0.102" MaterialId="human_naked" Position="-0.017,0.180"/>
833     <Shape Type="disk" Radius="0.140" MaterialId="human_naked" Position="0.010,0.079"/>
834     <Shape Type="disk" Radius="0.146" MaterialId="human_naked" Position="0.015,0.000"/>
835     <Shape Type="disk" Radius="0.140" MaterialId="human_naked" Position="0.010,-0.079"/>
836     <Shape Type="disk" Radius="0.102" MaterialId="human_naked" Position="-0.017,-0.180"/>
837   </Agent>
838   <Agent Type="pedestrian" Id="4" Mass="91.17" Height="1.83" MomentOfInertia="1.89" FloorDamping="2.00" AngularDamping
839     ↳="2.00">
840     <Shape Type="disk" Radius="0.088" MaterialId="human_naked" Position="-0.017,0.165"/>
841     <Shape Type="disk" Radius="0.122" MaterialId="human_naked" Position="0.010,0.073"/>
842     <Shape Type="disk" Radius="0.127" MaterialId="human_naked" Position="0.015,-0.000"/>
843     <Shape Type="disk" Radius="0.122" MaterialId="human_naked" Position="0.010,-0.073"/>
844     <Shape Type="disk" Radius="0.088" MaterialId="human_naked" Position="-0.017,-0.165"/>
845   </Agent>
846   <Agent Type="pedestrian" Id="5" Mass="87.54" Height="1.90" MomentOfInertia="1.90" FloorDamping="2.00" AngularDamping
847     ↳="2.00">
848     <Shape Type="disk" Radius="0.088" MaterialId="human_naked" Position="-0.017,0.173"/>
849     <Shape Type="disk" Radius="0.122" MaterialId="human_naked" Position="0.010,0.076"/>
850     <Shape Type="disk" Radius="0.127" MaterialId="human_naked" Position="0.015,-0.000"/>
851     <Shape Type="disk" Radius="0.122" MaterialId="human_naked" Position="0.010,-0.076"/>
852     <Shape Type="disk" Radius="0.088" MaterialId="human_naked" Position="-0.017,-0.173"/>
853   </Agent>
854   <Agent Type="pedestrian" Id="6" Mass="95.25" Height="1.73" MomentOfInertia="2.33" FloorDamping="2.00" AngularDamping
855     ↳="2.00">
856     <Shape Type="disk" Radius="0.104" MaterialId="human_naked" Position="-0.017,0.168"/>
857     <Shape Type="disk" Radius="0.143" MaterialId="human_naked" Position="0.010,0.074"/>
858     <Shape Type="disk" Radius="0.149" MaterialId="human_naked" Position="0.015,0.000"/>
859     <Shape Type="disk" Radius="0.143" MaterialId="human_naked" Position="0.010,-0.074"/>
860     <Shape Type="disk" Radius="0.104" MaterialId="human_naked" Position="-0.017,-0.168"/>
861   </Agent>
862   <Agent Type="pedestrian" Id="7" Mass="98.88" Height="1.68" MomentOfInertia="2.41" FloorDamping="2.00" AngularDamping
863     ↳="2.00">
864     <Shape Type="disk" Radius="0.104" MaterialId="human_naked" Position="-0.017,0.168"/>
865     <Shape Type="disk" Radius="0.143" MaterialId="human_naked" Position="0.010,0.074"/>
866     <Shape Type="disk" Radius="0.149" MaterialId="human_naked" Position="0.015,0.000"/>
867     <Shape Type="disk" Radius="0.143" MaterialId="human_naked" Position="0.010,-0.074"/>
868     <Shape Type="disk" Radius="0.104" MaterialId="human_naked" Position="-0.017,-0.168"/>
869   </Agent>
870 </Agents>

```

AgentDynamics.xml file

```

872 <?xml version="1.0" encoding="utf-8"?>
873 <Agents>
874   <Agent Id="0">
875     <Kinematics Position="1.115,0.362" Velocity="0.00,0.00" Theta="-0.29" Omega="0.00"/>
876     <Dynamics Fp="100.0,0.0" Mp="0.00"/>
877   </Agent>
878   <Agent Id="1">
879     <Kinematics Position="0.211,0.235" Velocity="0.00,0.00" Theta="-0.48" Omega="0.00"/>
880     <Dynamics Fp="100.0,0.00" Mp="0.00"/>
881   </Agent>
882   <Agent Id="2">
883     <Kinematics Position="0.239,0.920" Velocity="0.00,0.00" Theta="-0.16" Omega="0.00"/>
884     <Dynamics Fp="100.0,0.00" Mp="0.00"/>
885   </Agent>
886   <Agent Id="3">
887     <Kinematics Position="0.724,0.929" Velocity="0.00,0.00" Theta="0.35" Omega="0.00"/>
888     <Dynamics Fp="100.0,0.0" Mp="0.00"/>
889   </Agent>
890   <Agent Id="4">
891     <Kinematics Position="0.463,0.252" Velocity="0.00,0.00" Theta="-0.21" Omega="0.00"/>
892     <Dynamics Fp="100.0,0.0" Mp="0.00"/>
893   </Agent>
894   <Agent Id="5">
895     <Kinematics Position="0.437,0.709" Velocity="0.00,0.00" Theta="-0.36" Omega="0.00"/>
896     <Dynamics Fp="100.0,0.0" Mp="0.00"/>
897   </Agent>
898   <Agent Id="6">
899     <Kinematics Position="0.757,0.299" Velocity="0.00,0.00" Theta="-0.20" Omega="0.00"/>
900     <Dynamics Fp="100.0,0.0" Mp="0.00"/>
901   </Agent>
902

```

```

903 <Agent Id="7">
904   <Kinematics Position="1.039,0.875" Velocity="0.00,0.00" Theta="-0.07" Omega="0.00"/>
905   <Dynamics Fp="100.0,0.0" Mp="0.00"/>
906 </Agent>
907 </Agents>

```

AgentInteractions.xml file for $t = 9.9$ s

```

909 <?xml version="1.0" encoding="utf-8"?>
910 <interactions>
911   <Agent Id="0">
912     <Agent Id="3">
913       <Interaction ParentShape="2" ChildShape="4" TangentialRelativeDisplacement="-0.000715705,-0.000640808" Fn="
914         ↪ 1.21016,-1.3516" Ft="-0.675798,-0.605078" />
915     </Agent>
916     <Wall ShapeId="4" WallId="0" CornerId="5" TangentialRelativeDisplacement="6.63116e-21,2.03987e-05" Fn="
917       ↪ -10.1248,-1.14704e-14" Ft="-7.61778e-14,5.03933" />
918   </Agent>
919   <Agent Id="1">
920     <Agent Id="5">
921       <Interaction ParentShape="2" ChildShape="3" TangentialRelativeDisplacement="0.00015316,-0.000992966" Fn="
922         ↪ 10.22,1.57639" Ft="0.788194,-5.11002" />
923     </Agent>
924     <Agent Id="4">
925       <Interaction ParentShape="3" ChildShape="3" TangentialRelativeDisplacement="2.1114e-06,3.56781e-06" Fn="
926         ↪ -18.5823,10.9969" Ft="-2.56769,-4.33883" />
927     </Agent>
928   </Agent>
929   <Agent Id="2">
930     <Agent Id="5">
931       <Interaction ParentShape="0" ChildShape="1" TangentialRelativeDisplacement="-0.000122243,0.00122959" Fn="
932         ↪ -6.20337,-0.616724" Ft="-0.308362,3.10168" />
933     </Agent>
934   </Agent>
935   <Agent Id="3">
936     <Agent Id="7">
937       <Interaction ParentShape="4" ChildShape="4" TangentialRelativeDisplacement="-3.22373e-05,2.52169e-05" Fn="
938         ↪ -0.137911,-0.176305" Ft="-0.0881525,0.0689554" />
939     </Agent>
940   </Agent>
941   <Agent Id="4">
942     <Agent Id="6">
943       <Interaction ParentShape="3" ChildShape="4" TangentialRelativeDisplacement="4.14307e-08,8.3854e-08" Fn="
944         ↪ -21.8097,10.7757" Ft="0.10954,0.221705" />
945     </Agent>
946   </Agent>
947   <Agent Id="6">
948     <Wall ShapeId="0" WallId="0" CornerId="5" TangentialRelativeDisplacement="2.49307e-22,-5.00582e-06" Fn="
949       ↪ -31.8342,-8.49639e-15" Ft="-6.12397e-16,11.838" />
950   </Agent>
951 </interactions>
952

```

D Packing algorithm within the streamlit app

The `pack_agents_with_forces` method, detailed in Algorithm 1, simulates the arrangement of agents within a bounded environment by iteratively applying physics-inspired, force-based interactions to resolve overlaps and enforce boundary constraints. Additionally, a temperature-based cooling mechanism is used to gradually reduce the magnitude of rotation, helping the system to stabilise. The algorithm relies on the following forces:

Agent-agent repulsive force

For every pair of agents i and j , a repulsive force is computed that decays exponentially with the distance between their centroids:

$$\mathbf{F}_{i,j}^{\text{rep}} = \begin{cases} e^{-|\mathbf{r}_i - \mathbf{r}_j|/\lambda} \frac{\mathbf{r}_i - \mathbf{r}_j}{|\mathbf{r}_i - \mathbf{r}_j|} & \text{if } |\mathbf{r}_i - \mathbf{r}_j| > 0 \\ \text{random small vector} & \text{otherwise} \end{cases} \quad (\text{D.1})$$

where \mathbf{r}_i is the centroid of agent i and λ is the repulsion length.

Contact force

Algorithm 1: Agent packing with a force-based algorithm

```

1 Method pack_agents_with_forces(repulsion_length, desired_direction,
  variable_orientation):
2   foreach agent do
3     | RotateTo(agent, desired_direction)
4   end
5    $T \leftarrow 1.0$  ▷ Initial temperature
6   for iteration  $\leftarrow 1$  to MAX_NB_ITERATIONS do
7     foreach agent i do
8       forces  $\leftarrow [0, 0, 0]$  ▷ [x, y, rotation]
9       foreach agent j  $\neq i$  do
10        | forcesxy += repulsive_force(i, j, repulsion_length) ▷  $\mathbf{F}_{i,j}^{\text{rep}}$ 
11        | if overlap(i, j) then
12          | forcesxy += contact_force(i, j) ▷  $\mathbf{F}_{i,j}^{\text{contact}}$ 
13          | forcesrot += rotational_force(T) ▷  $f^{\text{rot}}$ 
14        | end
15      end
16      if boundary exists and (agent i is in contact with or outside the boundary)
17        | forces += boundary_forces(i, T) ▷  $\mathbf{F}^{\text{bound}}$ 
18      end
19      if variable_orientation then
20        |  $\theta_i \leftarrow \theta_i + \mathbf{forces}_{\text{rot}}$  ▷ Update orientation
21      end
22       $\mathbf{r}_{\text{new}} = \mathbf{r}_{\text{current}} + \mathbf{forces}_{\text{xy}}$  if valid_position( $\mathbf{r}_{\text{new}}$ ) then
23        |  $\mathbf{r}_i \leftarrow \mathbf{r}_{\text{new}}$  ▷ Update position
24      end
25    end
26     $T \leftarrow \max(0, T - 0.1)$  ▷ Cooling
27  end

```

967 If two agents' shapes overlap, a contact force is applied to push them apart:

$$\mathbf{F}_{i,j}^{\text{contact}} = \begin{cases} k \frac{\mathbf{r}_i - \mathbf{r}_j}{|\mathbf{r}_i - \mathbf{r}_j|} & \text{if } |\mathbf{r}_i - \mathbf{r}_j| > 0 \\ \text{random small vector} & \text{otherwise} \end{cases} \quad (\text{D.2})$$

968 where k is the contact intensity.

969

970 Rotational force

971 When rotational dynamics are enabled, a random angular adjustment is applied, scaled by the
 972 temperature T of the system:

$$f^{\text{rot}} = \text{Uniform}(-\alpha, \alpha) \cdot T \quad (\text{D.3})$$

973 where α is the maximum rotational intensity.

974

975 Boundary forces

976 If an agent is outside the boundaries or in contact with a force $\mathbf{F}^{\text{bound}}$ is computed to push it
 977 back inside, expressed as the sum of:

- 978 ★ a contact force (as above) between the agent's centroid and the closest point on the
- 979 boundary of the agent's centroid.
- 980 ★ a rotational force (as above), scaled by the current temperature.

981 E Writing style

982 To guarantee that our open-source platform, written in Python and C++, is of high quality
983 and easy to maintain, we use automatic checks called *pre-commit hooks*. These checks are
984 triggered each time code is committed or pushed to the Git repository, allowing us to identify
985 and address issues before any changes are integrated into the codebase. For the Python code,
986 the following tools are used:

- 987 ★ **Ruff [43]**: This tool reviews the code to catch common mistakes and ensures we follow
988 established Python programming practices. It performs *linting*, which involves, among
989 other checks, identifying logical errors, overly complex functions, undeclared variables,
990 and deprecated functions. It also handles *formatting*, which means automatically arrang-
991 ing the code—such as fixing indentation, spacing, and comments—so that it remains
992 consistently structured and easy to read.
- 993 ★ **Mypy [44]**: This tool verifies that the types of variables used in the code are consis-
994 tent—for example, ensuring that a variable defined as an integer remains an integer
995 throughout the program. It also verifies that the types used in the code match the type
996 information described in the function's documentation (type hints), helping to catch
997 mistakes where the wrong variable might be used or returned.
- 998 ★ **NumPydoc validation [45]**: It ensures each function docstring adheres to a clear and
999 standard format.
- 1000 ★ **Pytest**: This tool runs a series of small tests on the Python code (using the command `uv`
1001 run `pytest`). If any part of the code produces unexpected results or fails to work as
1002 intended, we are immediately alerted.

1003 For both Python and C++ code, we use:

- 1004 ★ **CodeSpell [46]**: It scans all the files and helps catch and fix common misspelt words.
1005 It does not check for word membership in a complete dictionary, but instead looks for a
1006 set of common misspellings.

1007 For the C++ code, we use:

- 1008 ★ **clang-format [47]**: This tool arranges the code according to the specific [formatting rules](#)
1009 [recommended by Google](#). Additionally, it places curly brackets according to the *Allman*
1010 style.
- 1011 ★ **clang-tidy [48]**: This tool analyses the C++ code to catch common programming mis-
1012 takes and potential bugs before the program runs. It identifies issues such as violations
1013 of coding style, incorrect use of interfaces (for example, calling functions in the wrong
1014 way), and typing errors that can be detected by examining the code without executing
1015 it (via static analysis).
- 1016 ★ **cpplint [49]**: This tool checks that the code follows all the [coding style guidelines rec-](#)
1017 [ommended by Google](#) for C++.

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